Greater Dalton MPO
201 South Hamilton Street, Dalton, GA 30720
Metropolitan Planning Organization (706) 876-2592

Public Hearing: December 7, 2023 - Joint Committee Meeting Minutes
Location: 1999 Riverbend Drive, Dalton, Georgia
Call to Order: 10:04 A.M.
Adjournment: 11:05 A.M.

## I. Presentations

## Presenter:

Discussion:

GDOT District 6 - Office of Planning

- Roundabout for SR 3 @ Five Springs Road and Old Dixie Highway
The group discussed the proposed roundabout at the intersection and what alternatives were considered. The MPO was invited to be part of the concept meeting, and voice concerns to the project design team. GDOT encouraged any comments regarding the proposed project be submitted before the concept meeting, so the design team would have time to review those concerns.

The traffic report and concept are attached at the end.

Presenter: City of Dalton
Discussion:

Discussion:

Presenter: Whitfield County Engineering Department

- Market Street Corridor:

Design for Phase II in progress.
Right-of-Way for Phase I still in negotiation.

- The Whitfield County Board of Commissioners voted to construct a roundabout at the intersection of Houston Valley Road and Mt. Vernon Road. The project is in design phase.
- The realignment of Dawnville Beaverdale Road and Beaverdale Road Intersection was completed by the Public Works Department. The New section is now open to the
public. A new signalized intersection, to the north, is in design phase.

Presenter:
Discussion:

## Greater Dalton Metropolitan Planning Organization

- Consideration to accept agreement with ChattanoogaHamilton County

The MPO must renew the MOU with ChattanoogaHamilton County to maintain current planning boundaries. The new agreement will reflect data from the 2020 Census.

- FY 2024-2027 Transportation Improvement Program

Two draft amendments will be brought before the Policy Committee to reflect updated funding amounts and codes for GDOT projects in the TIP.

## II. New Business

1) Action Item: Consideration to accept agreement with Chattanooga-Hamilton County Approved: Mayor Kenny Gowin made a motion to accept the continued agreement. Mayor Tom Dickson seconded the motion. The agreement passed on a $7-0$ vote.
2) Action Item: Amendments to the FY 2024-2027 Transportation Improvement Program Approved: Mayor Tom Dickson made a motion to approve the draft amendments. Mayor Kenny Gowin seconded the motion. The amendments passed on a $7-0$ vote.

## III. Adjournment

Kent Benson adjourned the meeting at 11:05 A.M.
Minutes submitted by: Jacob Bearden

## DEPARTMENT OF TRANSPORTATION STATE OF GEORGIA

TRAFFIC ENGINEERING STUDY
October 2021


PRIMARY ROUTE: SR 3
SECONDARY ROUTE: S DALTON BYPASS
MILEPOINT: N/A
GDOT DISTRICT: 6
CONGRESSIONAL DISTRICT: 14
COUNTY: WHITFIELD
CITY: DALTON
PREPARED BY: ARCADIS


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## STUDY REQUEST

Georgia Department of Transportation (GDOT) District 6 requested for a Traffic Engineering (TE) study at the intersection of State Route (SR) 3 and Old Dixie Highway/Five Springs Road due to the frequency of fatal and severe injury crashes observed at the intersection.

## PROJECT LOCATION

The project is located in the city of Dalton (Whitfield County) at the intersection of SR 3 and Old Dixie Hwy/Five Springs Rd. SR 3 is a four-lane rural major arterial that runs in the east-west direction with a posted speed limit of 55 MPH. Traffic in opposing direction along SR 3 is separated by paved median. Old Dixie Hwy is a two-lane rural major collector that connects traffic from the south to the intersection. The posted speed limit along Old Dixie Hwy is 50 MPH . Five Spring Rd is a two-lane rural local road that connects traffic from the north to the intersection. The posted speed limit along Five Springs Rd is 40 MPH . The intersection is stop controlled on the side streets (Five Springs Rd/Old Dixie Hwy). Land use within the vicinity of the intersection consists primarily of forest. The area view of the study location is shown in Figure 1.

## PROJECT JUSTIFICATION STATEMENT

The intersection at SR 3 and Old Dixie Hwy/Five Springs Rd was identified by GDOT District 6 Traffic Operations having observed fatal and severe injury collisions in recent years. For the 6 -year crash analysis period (2015-2020), the intersection recorded a total of 46 crashes, comprising of 1 fatal, 19 injury, and 26 property-damage only (PDO) collisions. The fatal crash was an angle collision between a NB passenger car (Veh \#1) and an EB passenger car (Veh \#2) on a clear day with dry road surface condition around 5 PM. Veh \#1 was attempting to cross SR 3 from the stop-controlled approach but failed to yield to Veh \#2 which had the right-of-way. Driver of Veh \#1 sustained fatal injury having been struck on the driver's front side by Veh \#2. Angle crashes at intersection represented approximately $37 \%$ ( 17 crashes) of the total crashes while rear-end crashes accounted for $39 \%$ ( 18 crashes) of the total crashes. The angle crashes occurred primarily due to at fault drivers' failure to yield to vehicles with the right-of-way as noted from the crash reports. Out of the 17 angle crashes, 8 were right-angle collisions involving two vehicles traveling perpendicular to each other and 9 were left-turn crashes involving left-turn vehicles and vehicles proceeding through the intersection. Left turn crashes were more prevalent on the SB approach compared to other approaches. Rear-end collisions were predominant on the NB channelized right turn approach. From the crash history reports, "following too closely" was cited as a major concern for rear-end collisions.

This current study seeks to investigate the safety concerns and propose safety countermeasures that are intended to reduce the high crash frequency and severity at the intersection. The study will provide an evidence-based comparison of intersection alternatives to justify the preferred intersection traffic control for mitigating the crash problems. The crash data is included in Appendix A.


Figure 1: Aerial view showing project location and study intersection

## FIELD VISIT

A field visit was completed on Friday, April 30, 2021, to observe, identify and document existing site and traffic conditions. The field visit observations included:
A. Intersection Control and Geometry:

The four-leg intersection is unsignalized. The mainline, SR 3, is free flow, while the side streets, 5 Springs Rd/Old Dixie Hwy, are stop controlled. The mainline has 2 through lanes, one left turn lane, and channelized right turn lanes (striped islands) on each approach. The sides streets have single lane with a slip right turn lane channelized with raised concrete island on each approach.
B. Horizontal/Vertical Grades: The intersection is relatively on a level ground with little or no vertical curves. There is a horizontal curve approximately 400 ft from the intersection on the northbound approach.
C. Intersection Delay / Queuing: During the field visit, no traffic queues were observed within the intersection. Traffic was free flowing along the mainline with minimal stop delays observed for vehicles on the side street. Travel speed on the mainline appear to be higher than posted speed limit, making it difficult for side street traffic to accept gaps to cross or make a left turn.
D. Sight Distance / Obstruction Concerns: No sight distance obstructions were observed within the intersections. Sight distances are adequate on all intersection approaches. Although not measured on the field, sight distances are adequate on all intersection approaches as noted in previous GDOT TE study.
E. Adjacent Signalized Intersection: The closest signalized intersection along SR 3 corridor west of the study location is at SR 3 and S Dixie Rd/US 41 (approximately 1.6 miles). To the east of the study intersection, approximately 1750 ft is the signalized intersection of SR 3 and Abutment Rd
F. Pavement/Signs/Striping Conditions: The pavement markings at intersection appeared adequate with minor wears. Field observations showed that the road signs are adequately maintained and highly visible. All right-turn maneuvers at the intersection are controlled with "YIELD" signs (R1-2). Through and left turn movements from the side streets are controlled by standard "STOP" signs (R1-1). from the EB and WB approaches are channelized and controlled with yield signs (R1-2).
G. Pedestrian Accommodations: There are no sidewalks and pedestrian crosswalks within the intersection.
H. Lighting: There are no overhead street lightings at the intersection.
I. Parking: There are no on-street parking accommodations at or near the intersection.
J. Potential Environmental Impacts: Based on field observations, several environmental concerns or impact of the project to existing utilities were noted. The impacts are further discussed in the environmental section of this report.
K. Other Modes of Transportation: There are no bus stops along the corridors.

## CRASH ANALYSIS

Six-years crash data (2015-2020) for the area of influence were obtained from Georgia Electronic Accident Reporting System (GEARS). Crash analysis was performed to quantify the frequency and severity of crashes within the project limit. The goal of the crash analysis was to understand the crash trends/patterns and identify improvements that have the greatest potential to address the safety concerns. Results from the crash analysis are highlighted below. Crash diagrams are included in Appendix B.

## Summary of Intersection Crashes

Table 1 summarizes the crash data by crash severity and manner of collisions at the intersection. For the 6-year period (2015-2020), the intersection experienced a total of 46 crashes including 1 fatal, 19 injury and 26 PDO crashes. Rear-end crashes were the most prevalent crash type at the intersection, followed by angle collisions. As shown in Table 1, angle crashes represented approximately 37\% (17 crashes) of the total crashes while rear-end crashes accounted for $39 \%$ ( 18 crashes) of the total crashes. The fatal collision was a right-angle crash between a NB through vehicle (Veh \#1) and an EB through vehicle (Veh \#2). Veh \#1 was attempting to cross SR 3 from the stop-controlled approach but failed to yield to Veh \#2 which had the right-of-way. Driver of Veh \#1 sustained fatal injury having been t-boned by Veh \#2. From the crash reports, the angle crashes within the intersection occurred primarily due to at fault drivers' failure to yield to vehicles that had the right-of-way. Out of the 17 angle crashes, 8 were right-angle collisions involving two vehicles traveling perpendicular to each other and 9 were left-turn crashes involving left-turn vehicles and vehicles proceeding through the intersection. From the breakdown of angle collisions (Table 2), left turn crashes appear to be more prevalent for the SB left turn maneuver compared to other intersection left turn movements. Rear-end collision is most predominant on the NB channelized right lane accounting for $83 \%$ (15 out 18) of all rear-end collisions at the intersection. According to police reports, "following too closely" was cited as the major contributory factor for the rear-end collisions. Using the Highway Safety Manual (HSM) methodology, intersections with similar characteristics typically experience 2.8 crashes per year. The crash rate at this intersection is considerably higher ( 7.7 crashes per year) compared to the rates observed at other intersections with similar geometry and traffic characteristics, hence the need for safety improvements at this location.

Table 1: Intersection Crash Summary (2015-2020)


ADT = average daily traffic; MEV = million entering vehicles
K=fatal injury; $A=$ Incapacitating injury; $B=$ Non-incapacitating injury; $C=P o s s i b l e ~ i n j u r y ; ~ O=N o ~ i n j u r y ~$
Table 2: Distribution of Angle Crashes by Maneuver and Crash Severity

| Maneuver (Vehicle \#1) | Injury <br> Severity | Maneuver (Vehicle \#2) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EBT | EBL | NBT | SB ${ }^{-1}$ | WBT |
| EBT | B |  |  | 1 |  |  |
| WBT | A |  |  |  | 1 |  |
| WBL | A | 1 |  |  |  |  |
|  | 0 | 1 |  |  |  |  |
| NBT | K | 1 |  |  |  |  |
|  | B | 2 |  |  |  |  |
|  | C |  |  |  |  | 1 |
|  | 0 | 1 |  |  |  | 1 |
| NBL | B | 1 |  |  | 1 |  |
|  | 0 |  | 1 |  |  |  |
| SBL | B |  |  | 1 |  |  |
|  | C |  |  | 1 |  |  |
|  | 0 |  |  | 2 |  |  |

## Time of the Day Analysis

Figure 2 displays the crashes by time of the day in relation to hourly traffic volumes and the lighting conditions within the study limit. As shown in Figure 2, the crashes were fairly distributed across the $24-h r$ period with peak crash frequencies observed at the morning ( 6 AM) and evening (5 PM) hours. The data shows a strong correlation between the crash frequencies and traffic volumes. Moreover, majority of the crashes ( $65 \%$ ) occurred during the daylight hours, with noticeable proportions (about $28 \%$ of total crashes) occurring during the "dark not lighted" hours.


Figure 2: Summary of Crashes by Time of Day, Lighting Condition and Hourly Vehicular Volume

## Seasonal Analysis

The number of crashes occurring each day of the week as well as the month of the year were analyzed to identify high crash frequency days and months. As shown in Table 3, the crashes were distributed fairly across the weekdays and across the months. The crash frequencies appear to be high in the Summers, especially in August, compared to the other months or seasons.

Table 3: Distribution of Crashes by Day of Week and Month of Year

| SEASON/ <br> Month | DAY OF WEEK |  |  |  |  |  |  | Total | Percent of Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Monday | Tuesday | Wednesday | Thursday | Friday | Saturday | Sunday |  |  |
| WINTER | 3 | 1 | 1 | 3 | 1 | 0 | 1 | 10 | 22\% |
| December | 1 | 1 | 1 | 1 |  |  | 1 | 5 | 11\% |
| January | 1 |  |  | 2 |  |  |  | 3 | 7\% |
| February | 1 |  |  |  | 1 |  |  | 2 | 4\% |
| SPRING | 3 | 1 | 2 | 1 | 2 | 1 | 1 | 11 | 24\% |
| March | 3 |  | 1 |  | 1 |  |  | 5 | 11\% |
| April |  |  | 1 |  | 1 |  | 1 | 3 | 7\% |
| May |  | 1 |  | 1 |  | 1 |  | 3 | 7\% |
| SUMMER | 1 | 4 | 1 | 2 | 2 | 2 | 2 | 14 | 30\% |
| June | 1 | 1 | 1 | 2 |  |  |  | 5 | 11\% |
| July |  | 3 |  |  |  |  |  | 3 | 7\% |
| August |  |  |  |  | 2 | 2 | 2 | 6 | 13\% |
| FALL | 1 | 2 | 4 | 0 | 2 | 1 | 1 | 11 | 24\% |
| September |  | 1 | 1 |  |  | 1 |  | 3 | 7\% |
| October | 1 | 1 |  |  | 1 |  | 1 | 4 | 9\% |
| November |  |  | 3 |  | 1 |  |  | 4 | 9\% |
| Total | 8 | 8 | 8 | 6 | 7 | 4 | 5 | 46 |  |
| Percent of Total | 17\% | 17\% | 17\% | 13\% | 15\% | 9\% | 11\% |  | \% |

## OPERATIONAL ANALYSIS

## Traffic Volume Counts

Twelve-hour (12-hr) intersection turning movement counts were collected at the intersection of SR 3 and 5 Springs Rd/old Dixie Hwy on Wednesday, October 9, 2019 from 6:00 AM to 6:00 PM. The counts included all cars, trucks or other motorized vehicles passing through the intersections. The traffic volume counts for the intersection is included in Appendix C.

## Existing Operations

A Synchro analysis was completed for the existing traffic and No Build conditions at the intersection. Results of the analysis are included in Appendix D and summarized below. Table 4 shows the results of the existing and No Build traffic operations at intersection.
Table 4: Existing \& No Build AM / PM Peak Hour Intersection Operations

| Approach | Existing (2019) |  |  |  | No Build (2024) |  |  |  | No Build (2044) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM |  | PM |  | AM |  | PM |  | AM |  | PM |  |
|  | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS |
| Old Dixie Hwy (NB) | 24.9 | C | 6.1 | A | 265.5 | F | 7.4 | A | 3488.5 | F | 1188.2 | F |
| 5 Springs Rd (SB) | 36.3 | E | 9.8 | B | 46.6 | E | 15.9 | C | 2310.8 | F | 1615.1 | F |
| SR 3 (EB)* | 4.0 | - | 3.0 | - | 4.4 | - | 3.2 | - | 24.9 | - | 4.0 | - |
| SR 3 (WB)* | 4.6 | - | 3.9 | - | 4.8 | - | 4.4 | - | 76.4 | - | 9.8 | - |
| Intersection | 6.4 | - | 4.1 | - | 23.4 | - | 4.8 | - | 105.7 | - | 85.4 | - |

*Free flow approach. Non-zero delay include delay for left and u-turns
As shown in Table 4, traffic operations on the side streets for the existing and No Build (2024) conditions appear to be stable in the PM peak hours compared to the AM peak hours, however, in the design year (2044), traffic operations deteriorate, with the side streets operating at LOS F.

## Warrant Analysis

The Manual of Uniform Traffic Control Devices 2009 Edition (MUTCD) is the established source for evaluating warrants for installing a traffic signal. The MUTCD establishes nine traffic signal warrants that define minimum conditions under which signal installations may be justified. A signal warrant analysis was performed based on existing 12 -hour turning movement counts at the intersections. The full warrant report is included in Appendix E. Table 5 shows the signal warrant analysis for the intersection. Based on the signal warrant analyses, the intersection does not meet any of the signal warrants at $100 \%$ volume threshold. Therefore, a signal is not warranted at this intersection.

Table 5: Summary of Current Conditions Signal Warrant Analysis


N/A = not applicable

## INTERSECTION CONTROL EVALUATION (ICE)

Georgia Department of Transportation's Intersection Control Evaluation (ICE) policies were developed to further leverage safety advancements as part of intersection improvements for the study intersection. The ICE process consists of two distinct stages. Stage 1 identifies potential intersection control types that may provide safety benefits based on the existing conditions. Stage 2 further evaluates those alternatives inclusive of safety, operations, cost, environmental impacts, and project support. The following alternatives were evaluated in Stage 2 for the intersection. The ICE results are included in Appendix F and the operational analyses for each alternative are also included in Appendix G. Two intersection alternatives were evaluated including a multi-lane roundabout, and an RCUT.

## Multi-lane Roundabout

A multi-lane roundabout was evaluated for this intersection because it would provide fewer conflict points than the existing configuration. This alternative would also decrease the crash frequency and severity while increasing operational efficiency and reducing speeds for vehicles entering the intersection. The multi-lane roundabout would help mitigate the 9 left-turn and 8 right-angle crashes by removing opposing conflict points since drivers are expected to travel in the same direction through the circulatory roadway. Based on Federal Highway Administration (FHWA) crash modification factors, the installation of a multi-lane roundabout at this location is anticipated to reduce the occurrence of fatal/injury and PDO collisions by $87 \%$ and $71 \%$, respectively, for all crash types. The annual safety benefit cost for this alternative is 13.2. This alternative ranked first in the ICE Stage 2 analysis with a score of 6.4. The total cost for the multi-lane roundabout is estimated to be $\$ 2,405,000$.

## Restricted Crossing U-turn (RCUT)-Stop Control

An unsignalized Restricted Crossing U-turn (RCUT-stop control) would reduce the 32 conflict points at existing intersection to 9 points and would provide substantial safety benefits with moderate increase in delay for the side street traffic. This alternative would restrict left-turn and through movements from the side streets (5 Springs Rd/Old Dixie Hwy), potentially mitigating the 14 angle collisions that occurred between the side street vehicles and vehicles on the mainline (SR 3). Based on Federal Highway Administration (FHWA) crash modification factors, the installation of an RCUT is anticipated to reduce the occurrence of fatal/injury and PDO collisions by $54 \%$ and $43 \%$, respectively, for all crash types. The estimated construction cost for this alternative is $\$ 1,100,000$. The annual safety benefit cost for this alternative is 16.3. The RCUT ranked second in the stage 2 analysis of the ICE with a score of 5.6.

## Intersection Crash Reduction Factors

The Crash Reduction Factors (CRF) used in the ICE Stage 2 analysis were determined from the FHWA's Crash Modification Factors Clearinghouse website (http://www.cmfclearinghouse.org/) and are provided in Table 4 below.

Table 6: Intersection Crash Reduction Factors

| Alternative | PDO | Fatal//njury |
| :--- | :---: | :---: |
| Multi-lane Roundabout | $71 \%$ | $87 \%$ |
| RCUT | (CMF ID: 229 ) | (CMF ID: 230) |

## EXPECTED OPERATIONAL RESULTS

The intersection delay and LOS results for the design year (2044) for all alternatives considered in the ICE Stage 2 analysis are summarized in Table 5. The analysis reports are also provided in Appendix G.

As shown in Table 5, the RCUT alternative would provide higher intersection operational benefits compared to the multi-lane roundabout, however, the delay for the left-turn vehicles on the minor streets would increase significantly. Operationally, the RCUT would require through and left turn vehicles to first turn right at the main intersection and then execute left turns by making U-turns at the median opening downstream of the intersection. Once the drivers make U-turns, they then must turn right or proceed through the intersection when they reach the cross street, hence, increasing the travel time for left and through vehicles from the side street. Although the multi-lane roundabout will increase delay for mainline through vehicles compared to the RCUT alternative, it will minimize the delay for left turn and side street through vehicles.

Table 7: Operational Results for Alternatives (Design Year 2044)

| Approach | NO BUILD |  |  |  | Alternative 1: <br> Single-lane Roundabout |  |  |  | Alternative 2: RCUT |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM |  | PM |  | AM |  | PM |  | AM |  | PM |  |
|  | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS | Average Delay (sec) | LOS |
| Old Dixie Hwy (NB) | 3488.5 | F | 1188.2 | F | 43.9 | E | 14.7 | B | 13.8 | B | 3.6 | A |
| 5 Springs Rd (SB) | 2310.8 | F | 1615.1 | F | 11.3 | B | 11.9 | B | 1.5 | A | 3.6 | A |
| SR 3 (EB)* | 24.9 | - | 4.0 | - | 11.4 | B | 8.1 | A | 2.8 | - | 1.4 | - |
| SR 3 (WB)* | 76.4 | - | 9.8 | - | 11.4 | B | 8.0 | A | 4.0 | - | 2.9 | - |
| Intersection | 105.7 | - | 85.4 | - | 14.2 | B | 8.8 | A | 4.3 | - | 2.5 | - |

*Free flow approach. Non-zero delay include delay for left and u-turns

## SAFETY BENEFIT-COST ANALYSIS

A summary of the safety benefit cost ( $B / C$ ) ratios for the alternatives considered is presented in Table 6. Construction cost estimates for the preferred alternative is also included in Appendix H. Details of the B/C ratio calculations are included in Appendix I.

## Table 8: Intersection Safety Countermeasures Benefit/Cost Ratios

| Safety Countermeasure | Estimated Construction <br> Costs | B/C Ratio |
| :--- | :---: | :---: |
| Multi-lane Roundabout | $\$ 2,405,000$ | 13.2 |
| RCUT | $\$ 1,100,000$ | 16.3 |

## PROJECT RISK ANALYSIS

This section identifies potential risks that could delay recommended improvements at the intersection. These risks include environmental impacts, utility conflicts, and other corridor issues. The goal of identifying these potential risks as part of this traffic study is to prevent project delays once improvements have been selected for delivery.

## Environmental Screening

To assist GDOT in understanding the potential environmental constraints within the corridor, Arcadis staff conducted a desktop survey using National Wetland Inventory (NWI) maps, Georgia's Natural, Archaeological, and Historic Geographic Information System (GNAHRGIS), the U.S. Environmental Protection Agency's (USEPA) EnviroMapper, and the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps (FIRM) for identifying environmental resources that may be afforded protection under the National Environmental Policy Act (NEPA). The environmental screening report is included in Appendix J. The screening findings are summarized below:

- Five historic properties that may be afforded protection under Section 4(f) were identified within and adjacent to the project limits. Coordination and a Historic Resources Survey Report by a certified historian would be necessary to confirm the full extent of historic resources and their eligibility for listing in the National Register of Historic Places (NRHP)
- 3092 Five Springs Rd, 1961
- 3072 Five Springs Rd, 1961
- 3051 Five Springs Rd, 1961 (GNAHRGIS data point)
- 3067 Five Springs Rd, 1961
- 3073 Five Springs Rd, 1961
- The proposed project is adjacent to forested areas within the range of the Gray Bat. The impact of the project on the protected species and their habitat may be need.
- Portion of the study corridor contains a flood zone or flood hazard area. Coordination with project engineers and designers is necessary to confirm the location of the floodplain and any impacts resulting from the proposed project's design

A utility cost estimate with GDOT was not completed in this study. However, based on field observations, it was determined that project would likely impact electrical, gas and water distribution lines as shown in the pictures below taken from site visit.


Electrical lines (SW quadrant of intersection)


Water lines/Hydrant (SE quadrant of intersection)


## Other Projects

Using GeoPI, two maintenance construction projects were identified along SR 3 corridor.

- PI M005644: Resurfacing of SR 3 from SR 3 Conn to CR 666/Old Dixie Hwy (93.59\% construction complete)
- PI M005635: Resurfacing of SR 3 from CR 666/Old Dixie Hwy to SR 52 (90.28\% construction complete)


## CONCLUSION

Based on crash data from 2015 to 2020, the intersection at SR 3 and 5 Springs Rd/Old Dixie Hwy has recorded a total of 46 crashes including 1 fatal, 19 injury and 26 PDO crashes. Rear-end crashes were the most prevalent crash type at the intersection, followed by angle collisions. From the crash reports, the angle crashes within the intersection occurred primarily due to at fault drivers' failure to yield to vehicles that had the right-of-way. Out of the 17 angle crashes, 8 were right-angle collisions and 9 were left-turn crashes. Left-turn angle crashes appear to be major concern for the NB approach.

As discussed throughout the report, the proposed intersection improvements are expected to provide some of the highest crash mitigation and operational benefits. The preferred alternative (multi-lane roundabout) is anticipated to reduce fatal/injury and PDO crashes by $87 \%$ and $71 \%$, respectively. Similarly, a reduction of $54 \%$ and $43 \%$, respectively, for fatal/injury and PDO crashes are expected with the RCUT alternative. Although the RCUT alternative showed the lowest overall intersection delay, the delays for left turn movements from the side street were significantly higher compared to the multi-lane roundabout alternative. Besides reducing the speeds of vehicles entering the intersection, the turbo
features of the multi-lane roundabout would help eliminate weaving or changing lanes as drivers are expected to choose the correct lane before entering the roundabout.

## Recommendations

Based on the observed crash frequencies and severities, it is recommended that a multi-lane roundabout be programmed to be installed at the intersections of SR 3 and 5 Springs Rd/Old Dixie Hwy. Table 7 shows the intersection recommended safety improvement for the intersection with its delivery mechanism. The existing condition and proposed layout sketch of the preferred alternative are included in Appendix K. The TE study previously completed by GDOT is included in Appendix L.

Table 9: Intersection Safety Improvements Delivery Mechanisms

| Safety Improvement | Project Costs | B/C ratio | Delivery Method |
| :--- | :--- | :---: | :---: |
| Multi-lane roundabout | PE: $\$ 705,000$ <br> UTL: $\$ 100,000$ <br> ROW: $\$ 0$ <br> Const: $\$ 1,600,000$ <br> Total: $\$ 2,405,000$ | 13.2 | MOSD |



## Appendix A: Crash Data

| AccideniNo | Date | Time | crasisever | Manneorctolision | Light | Surace | Diverager | Divectage | vehrypel | Vehryeer | Dirven1 | Dirven2 | Mnwven1 | Mnveren2 | Numberonenicles | Latoesmal | Longpecimal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{5}^{5151884}$ | 1／29／2015 | ${ }^{7} 7.50 .00$ | $\bigcirc$ | Rear End | Dayiligh | Dry | ${ }^{34}$ | ${ }^{16}$ | ${ }^{\text {Passenger Car }}$ | Passenger Car | North | North | Turning Right | ${ }^{\text {stopped }}$ | ${ }_{2}^{2}$ | ${ }^{34.7019195}$ | ${ }^{-84.96663}$ |
| ${ }_{53682438}^{52425}$ | ${ }_{\text {4／5／2015 }}^{7 / 212015}$ | 20：5900 | ${ }_{8}^{8}$ | ${ }_{\text {Angle }}^{\text {Angle }}$ | DarkNot Lighted Daylight | ${ }_{\text {ory }}^{\text {ory }}$ | 73 39 | ${ }_{43}^{56}$ | Passenger Car Van | Sports Ulility Velicle（ SUV） Soorst utily | $\underbrace{}_{\substack{\text { North } \\ \text { South }}}$ | $\underbrace{\substack{\text { North }}}_{\text {South }}$ | Turing Left | $\underbrace{\text { a }}_{\substack{\text { Straight } \\ \text { Strabht }}}$ | 2 | ${ }_{\text {34，}}^{34.720216}$ | ${ }_{\text {－}}^{\text {－84，967046 }}$ |
| 5368838 <br> 540231 | 7／21／2015 | \％6．33：00 <br> $13: 44: 00$ | ${ }_{8}^{8}$ | Angle | － $\begin{aligned} & \text { Dayilight } \\ & \text { Daylight }\end{aligned}$ | Dry | 39 | ${ }_{23}^{43}$ | $\mathrm{V}_{\text {Van }}^{\text {Sorts Uutility Vehicle（SUV）}}$ | Sports Uulity Velicle（ SUV） Soorst Uutiry yehice（suy） | South | North | Turing Left | Straight | 2 | （34．7205 | $-84.966892$ |
| 5400361 546216 | ${ }^{8 / 2 / 2 / 2015}$ |  | ${ }^{\text {c }}$ | ${ }^{\text {Angle }}$ Notalision with Motor Vehicle | ${ }_{\text {Day }}^{\text {Daylight }}$ DarkNot Lighted | ${ }_{\text {dry }}^{\text {dry }}$ | 40 26 | ${ }^{23}$ | Sports Utilit Vehicle（SUV） Passenger car | Sports Uulity Vehicle（SUV） | South North | North | $\underset{\text { Turring Left }}{\text { Legratine }}$ | $\underbrace{\text { chen }}_{\substack{\text { Straight } \\ N / A}}$ | ${ }_{1}^{2}$ | 34．701973 ${ }_{34}$ | $\begin{aligned} & -84.96684 \\ & -84.96693 \end{aligned}$ |
| 5464216 | cole $\begin{aligned} & \text { 10111／2015 } \\ & 11 / 42015\end{aligned}$ |  | － | Nota Collision with Motor Vehicle Rear End | DaakNot Lighted Daylight | ${ }_{\text {dry }}$ | 26 26 | -1 30 | $\underset{\substack{\text { Passenger car } \\ \text { Passenger car }}}{ }$ | ${ }_{\substack{\text { Plickup Truck }}}^{\text {N／}}$ | North North | $\underset{\text { N／A }}{\text { North }}$ | Negotititin A A Cure Turing Right | ${ }_{\text {Stopeed }}$ | 2 | － $\begin{aligned} & 34.70206 \\ & 34.701953\end{aligned}$ | -84.96693 -84.96674 |
| 5497568 <br> 550647 | 111／4／2015 |  | $\bigcirc$ | Rear End Not $A$ colisison with Motor vehicle | Daylight Daylight | ${ }_{\text {dry }}^{\text {dry }}$ dry | － 32 | 30 -1 | ${ }_{\substack{\text { Passenger } \\ \text { Passenger car } \\ \\ \text { ar }}}$ | P／A Prichu Truck | Norrn | ${ }_{\text {North }}$ | Turning Right Straight | Stopeed | ${ }_{1}$ | ${ }_{34.702056}$ | ${ }_{-84.96934}^{-8.9674}$ |
| 5531848 | 1016／2015 | 11：01：00 | － | Sidiessipe．Same Direction | Dayilight | Dry | 40 | 0 | Passenger Car | Tractor／Trailer | South | South | Changing Lanes | Straight | 2 | 34.702056 | －84，966883 |
| 5767146 | 4／1／2016 | 4：53：00 | 8 | NotA collision with Motor Vehicle | DarkNot Lighted | Wet | ${ }^{38}$ | －1 | Passenger Car | N／A | South | N／A | Straight | N／A | 1 | ${ }^{34.70214}$ | －84，966564 |
| 5917302 | 9／13／2016 | 6．40000 | $\bigcirc$ | Angle | DarkNot Lighted | bry | ${ }^{60}$ | 54 | Van | Spors Uutilit Vehicle（SUV） | South | North | Turring teft | Straight | 2 | 34.701808 | －84．966728 |
| 6149505 | 3／13／2017 | 6：10．00 | $\bigcirc$ | Rear End | DarkNot Lighted | Dry | 46 | 46 | Passenger Car | Sports Uutilty velicle（SUV） | North | North | Turning Right | Stopped | ${ }_{2}$ | ${ }^{34.70181}$ | －84．9669 |
| 6158410 | 3／20／2017 | 16：52：00 | $\bigcirc$ | Rear End | Dayilight | Dry | 0 | 50 | Pickup Truck | Passenger Car | North | North | Backing | Turring Right | 2 | ${ }^{34.701736}$ | －84．96741 |
| 6272791 | 6／12／2017 | 9：27：00 | c | Not A colision with Motor vehicle | Daylight | Dry | 40 | －1 | Sports utilitr Venicle（SUV） | N／A | Esast | N／A | Straight | N／A | 1 | 34.702189 | －84．967178 |
| 6342159 | 8／5／2017 | 10：54：00 | 。 | Rear End | Davilight | Dry | ${ }^{26}$ | ${ }^{62}$ | Pickup Truck | Pickup Truck | North | North | Straight | Stopped | 2 | ${ }^{34.70176}$ | －84．9674 |
| ${ }_{\substack{6432561 \\ 6557213}}$ | 10171／2017 | 16：1：100 | $\bigcirc$ | Angle | $\underbrace{}_{\substack{\text { Daplight } \\ \text { Darkot Lighted }}}$ | ${ }_{\text {ory }}^{\text {dry }}$ | ${ }^{26}$ | ${ }^{23}$ | Passenger car Pickup ruck | Sporst Uutity Velicel（SUV） Soors utily vehice（suy） | South | North | ${ }_{\text {Tursing }}$ Teft | $\underbrace{}_{\substack{\text { stright } \\ \text { strabt }}}$ | 2 | （ $\begin{aligned} & 34.72021 \\ & 3470205\end{aligned}$ | -8.9 .9653 -84.96889 |
| ${ }_{6664288}^{65873}$ | ${ }_{\substack{\text { 1／2512018 } \\ 3 / 21 / 218}}$ |  | ${ }_{\text {B }}^{\text {a }}$ | ${ }_{\text {Angie }}^{\text {Angle }}$ | Datkot Lighted | Dry | 31 49 | 34 52 | ${ }_{\text {Premer }}^{\text {Pickup Truck }}$ Passenge Car |  | ${ }_{\substack{\text { West } \\ \text { East }}}^{\text {cest }}$ | $\underset{\substack{\text { East } \\ \text { North }}}{ }$ | Turning Left Straight | ${ }_{\substack{\text { Straight } \\ \text { stright }}}^{\text {Sta }}$ | ${ }_{2}^{2}$ | －${ }_{\text {34，702052 }}$ | ${ }_{\text {－}}^{\text {－84，} 4.9668889}$ |
| 6714617 | 5／15／2018 | 7．52：00 | － | Rear End | Daylight | Dry | ${ }_{63}$ | 45 | Pickup Truck | Sports Utility veicice（SUV） | North | North | Turning Right | Stopped |  | 34.701995 | ${ }_{-84.9659}$ |
| 6724009 | 5／24／2018 | 17：19：00 | c | Rear End | Daylight | Dry | 32 | 25 | Sports utility Venicle（SUV） | Pickup Tuck | North | North | Turning Right | Turring Right | 2 | ${ }^{34} 4.702087$ | ${ }_{-84.96991}$ |
| 6745549 | 6／13／2018 | 7：05：00 | ${ }^{8}$ | Angle | Daylight | Dry | 27 | ${ }^{30}$ | Passenger Car | Passenger Car | North | East | Turring left | Staight | ${ }^{3}$ | ${ }^{34.720003}$ | －84．968865 |
| 6770830 693340 |  |  | ${ }^{8}$ | ${ }^{\text {Angle }}$ Notilision with Motor Vehicle | Daylight dawn | Dry Ory | ${ }_{60}^{62}$ | ${ }_{-1}^{24}$ | ${ }_{\text {Passenger Car }}^{\text {Tractror }}$ | ${ }_{\text {Passenger Car }}$ | $\substack{\text { Norrh } \\ \text { East }}$ | $\underset{\substack{\text { East } \\ \text { N／A }}}{\text { cen }}$ | $\underbrace{\text { Ste }}_{\substack{\text { Straight } \\ \text { Stright }}}$ | $\underset{\substack{\text { Straibht } \\ N / A}}{ }$ | ${ }_{1}^{2}$ |  | －84．96686 -84.96796 |
| 7073523 | 2／1／2019 | 6：52：00 | － | Angle | Daylight | Dry | 19 | 59 | Passenger Car | Passenger Car | North | East | Turring left | Turning Left | 2 | ${ }^{34.70247}$ | －84．9672 |
| ${ }_{71126771}^{713968}$ |  | ${ }_{\text {c }}^{\text {8，06：00 }}$ | $\bigcirc$ | Angle Rear fod | Sayligh | ${ }_{\text {Wet }}^{\text {Wet }}$ | ${ }_{31}^{24}$ | 34 33 |  |  | West | $\underset{\substack{\text { East } \\ \text { North }}}{\text { ate }}$ | Turing Left | ${ }_{\substack{\text { Stright } \\ \text { Staped }}}$ | 2 | 34.701786 34701627 | ${ }_{-849.9665}^{-89688}$ |
| ${ }_{7189518}$ |  | 17：11：00 | ${ }_{8}$ | ${ }_{\text {Rearlt }}$ Angle | ${ }^{\text {deam }}$ | ${ }_{\text {Wery }}$ | ${ }_{43}$ | ${ }_{32}$ | －Pissengerar ${ }^{\text {Pickup Tuck }}$ | Sicken | North | ${ }_{\substack{\text { Nornh } \\ \text { East }}}^{\text {Nors }}$ | Stater | Steren ${ }_{\text {Staight }}$ | ${ }_{3}$ | ${ }^{34.406221}$ | ${ }_{-84.96693}$ |
| 7213258 | 5／18／2019 | 11：10：00 | A | Angle | Daylight | ory | 44 | ${ }_{41}$ | Passenger Car |  | West | cout | Stay |  | ${ }_{2}$ | ${ }_{34,702051}^{34011}$ | ${ }_{-84.966889}$ |
| ${ }^{2388760}$ | 6／6／2019 | 6：35：00 |  | Rear End | Dawn | dry | ${ }^{27}$ | 52 | Passenger Car | Pickup Tuck | North | North | Straight | stopped | 2 | ${ }^{34.70211}$ | －84．9636 |
| 725329 | 6／13／2019 | 1773000 | k | Angle | Dayilight | Dry | ${ }^{33}$ | 52 | Passenger Car | Passenger Car | North | East | Straight | Straight | 2 | 34.702051 | －84．966889 |
| ${ }_{7295765}$ | 7／23／2019 | 17：09：00 | $\bigcirc$ | Rear End | Davilight | Dry | ${ }^{40}$ | 54 | Passenger Car | Sports Utility Vehicle（SUV） | North | North |  | Turring Right | ${ }^{2}$ | ${ }^{34.72026}$ |  |
| 74453121 747202 | 11120／2019 |  | ${ }_{0}$ | ${ }_{\text {Nata }}$ Not Collision with Motor Vehicle | ${ }_{\text {Day }}^{\substack{\text { Daylight } \\ \text { Darkot Lighted }}}$ | Dry Dry | ${ }_{20}^{19}$ | ${ }_{22}$ | Passeneger Car Passenger Car |  | West | $\underset{\text { cast }}{\text { N／A }}$ | ${ }_{\substack{\text { Straight } \\ \text { Stright }}}^{\text {Ster }}$ | ${ }_{\text {Straight }}^{\text {N／A }}$ | $\frac{1}{2}$ | 34．701976 | ${ }_{-84.968889}$ |
| 7488081 | 12／11／2019 | 17：08：00 | c | ${ }_{\text {Rear End }}$ | Daylight | Dry | ${ }_{23}^{20}$ | ${ }_{60}$ | Sporss utility Vehicle（SUV） | Sassenger car | North | ${ }_{\text {cost }}^{\text {costh }}$ | Turning Right | ${ }_{\text {Staped }}$ | ${ }_{2}^{2}$ | ${ }_{344.7207}^{34.0207}$ | ${ }_{\text {－84，}}$ |
| 788179 | 12／15／2019 | 6：45：00 | c | Angle | DarkNot Lighted | Dry | 55 | ${ }^{43}$ | Passenger Car | Passenger Car | North | West | Straight | Straight | 2 | 34.702407 | －84．9679 |
| ${ }_{7}^{788392525}$ | 12／17／2019 | 19：13：00 | ${ }^{8}$ | Not A Collision with Motor Vehicle | DarkNot Lighted | Dry | ${ }^{28}$ | $-1$ |  | N／A | North | N／A |  | N／A | 1 | 34.7019 | －84．96786 |
| 7588535 7585029 | （2／124／2020 | 17：0：000 23：0700 cose | － |  | DarkNo Lighted <br> Darkot lighted | $\underset{\substack{\text { Wet } \\ \text { Wet }}}{\text { cet }}$ | 24 21 24 | 62 21 |  | Passenger Car <br> Passenger Car | $\underset{\substack{\text { East } \\ \text { North }}}{\text { Nose }}$ | $\underset{\substack{\text { cast } \\ \text { North }}}{\text { cen }}$ | $\underset{\substack{\text { Turring Right } \\ \text { Turning Right }}}{ }$ | $\underset{\substack{\text { Stopped } \\ \text { Stoped }}}{ }$ | ${ }_{2}^{2}$ | 34.702076 <br> 34.7202 | －84．9674 <br> -84.9624 |
| 7680953 | 8／1／6／2019 | 18：35：00 | 。 | Rear End | Daxlight | Dry | 24 | ${ }_{42}$ | Sporst Uutility Vehicle（SUV） | Sporss utility vehicle（SUV） | North | North | Surningight | ${ }_{\text {Ster }}^{\substack{\text { stopeed } \\ \text { Stright }}}$ | 2 | ${ }_{344.70193}$ | ${ }_{-84.96667}$ |
| 7697301 | 7／14／2020 | 8．51：00 |  | Not A Collision with Motor vehicle | Daylight | Dry | 37 | －1 | Single Unit Truck | N／A | Esat | N／A | Negotititing $A$ Cuve | N／A | 1 | 34.701726 | －84，966726 |
| 7722459 | 8／30／2019 | 12：13：00 | 。 | Rear End | Daylight | Dry | 38 | 44 | Passenger car | Passenger Car | South | South | ${ }_{\text {Straight }}$ | Straight | 2 | ${ }_{34,702588}$ | ${ }_{-84.967171}$ |
| 772487 | 9／72019 | 18：37：00 | － | Not A collision with Motor vehicle | Daylight | Dry | 18 | －1 | Passenger Car | N／A | North | N／A | Straight | N／A | 1 | 34.702238 | －84，966074 |
| ${ }_{7773569}^{77295}$ | 9／1／5／2019 | 19：42：00 192000 10， | $\bigcirc$ | Rear End Angle den | Dusk Davieht | ory | ${ }_{45}^{22}$ | ${ }_{40}^{42}$ | ${ }_{\substack{\text { Pickup Truck } \\ \text { Plicupup Tuck }}}$ | Passenger Car Passenger car | $\underset{\substack{\text { North } \\ \text { North }}}{\text { a }}$ | $\underbrace{\text { West }}_{\text {North }}$ | Turing Right | $\underbrace{\text { Ste }}_{\substack{\text { Stoped } \\ \text { Straight }}}$ | ${ }_{2}^{2}$ | 34．701969 |  |
| 7757003 | ${ }_{8}^{8 / 30 / 202020}$ | 21：04：00 | 。 | ${ }^{\text {Angle }}$ Collision with Motor vehicle | DarkNot Lighted | Wet | ${ }_{-1}$ | ${ }_{-1}$ | Sporst utility venicle（SUV） | N／A | North | N／A | Negotitaing A Curve | N／A | ${ }_{1}$ | ${ }_{34,701463}$ | ${ }_{-84.96621}$ |
| 7802796 | 10／5／2020 | 17：02：00 | － | Rear End | Dayiligh | Dry | 30 | 52 | Pickup Tuck | Pickup Truck | South | North | Turning Right | Stopped | 2 | 34．70224 | 84，9672 |
| 7888215 | 12／14／2020 | 15：45：00 |  | Rear End | Daylight | Dry | 37 | 26 | Passenger Car | Passenger Car | North | North | Turning Right | Stopped | 2 | 34.70188 | －84．9681 |

## Appendix B: HSM Crash Prediction



## Appendix C: Intersection Crash Diagram



## Appendix D: Traffic Data

All Traffic Data
ㄱ - - =-nexiolo11
(303) 216-2439
www.alltrafficdata.net

Location: \#4 Old Dixie Hwy \& SR 3 AM
Date and Start Time: Wednesday, October 9, 2019
Peak Hour: 07:00 AM - 08:00 AM
Peak 15-Minutes: 07:45 AM - 08:00 AM


Note: Total study counts contained in parentheses.
Traffic Counts

| Interval | SR 3 <br> Eastbound |  |  |  | SR 3 <br> Westbound |  |  |  | Old Dixie Hwy Northbound |  |  |  | 5 Springs Rd Southbound |  |  |  | Total | Rolling Hour | Pedestrain Crossings |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  | West | East | South | North |
| 6:00 AM | 0 | 7 | 59 | 1 | 0 | 14 | 91 | 2 | 0 | 3 | 6 | 35 | 0 | 1 | 4 | 2 | 225 | 1,601 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 20 | 110 | 6 | 0 | 28 | 139 | 3 | 0 | 1 | 0 | 29 | 0 | 2 | 2 | 1 | 341 | 1,874 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 20 | 164 | 11 | 0 | 47 | 209 | 7 | 0 | 1 | 1 | 38 | 0 | 1 | 0 | 6 | 505 | 1,981 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 30 | 170 | 8 | 0 | 64 | 196 | 7 | 0 | 1 | 2 | 41 | 0 | 1 | 6 | 4 | 530 | 2,065 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 10 | 208 | 3 | 0 | 37 | 163 | 8 | 0 | 5 | 6 | 49 | 0 | 2 | 0 | 7 | 498 | 2,155 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 9 | 171 | 5 | 0 | 31 | 187 | 5 | 0 | 3 | 0 | 29 | 0 | 2 | 1 | 5 | 448 | 2,130 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 26 | 223 | 3 | 0 | 29 | 247 | 7 | 0 | 3 | 2 | 43 | 0 | 1 | 0 | 5 | 589 | 2,070 | 0 | 0 | 0 | 2 |
| 7:45 AM | 0 | 34 | 237 | 1 | 0 | 32 | 251 | 12 | 0 | 1 | 3 | 43 | 1 | 2 | 0 | 3 | 620 | 1,749 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 25 | 227 | 2 | 0 | 27 | 149 | 9 | 0 | 1 | 0 | 26 | 0 | 4 | 0 | 3 | 473 | 1,376 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 11 | 177 | 2 | 0 | 15 | 142 | 4 | 0 | 1 | 3 | 23 | 0 | 2 | 0 | 8 | 388 | 1,127 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 12 | 105 | 1 | 0 | 17 | 94 | 1 | 0 | 4 | 4 | 20 | 0 | 4 | 0 | 6 | 268 | 985 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 11 | 117 | 1 | 0 | 20 | 74 | 1 | 0 | 2 | 1 | 16 | 0 | 2 | 0 | 2 | 247 | 917 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 9 | 83 | 4 | 0 | 16 | 83 | 0 | 0 | 1 | 3 | 16 | 0 | 1 | 3 | 5 | 224 | 889 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 6 | 95 | 1 | 0 | 15 | 97 | 3 | 0 | 3 | 2 | 17 | 0 | 1 | 1 | 5 | 246 | 849 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 4 | 71 | 3 | 0 | 12 | 77 | 2 | 0 | 3 | 1 | 21 | 0 | 1 | 1 | 4 | 200 | 814 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 5 | 76 | 4 | 0 | 11 | 84 | 5 | 0 | 3 | 3 | 19 | 2 | 1 | 2 | 4 | 219 | 861 | 0 | 0 | 0 | 0 |
| 10:00 AM | 0 | 4 | 71 | 5 | 0 | 12 | 60 | 2 | 0 | 0 | 1 | 17 | 0 | 7 | 0 | 5 | 184 | 851 | 0 | 0 | 0 | 0 |
| 10:15 AM | 0 | 4 | 69 | 4 | 0 | 18 | 87 | 4 | 0 | 2 | 4 | 15 | 0 | 1 | 1 | 2 | 211 | 895 | 0 | 0 | 0 | 0 |
| 10:30 AM | 0 | 7 | 93 | 1 | 0 | 8 | 96 | 2 | 0 | 4 | 4 | 22 | 0 | 1 | 3 | 6 | 247 | 934 | 0 | 0 | 0 | 0 |
| 10:45 AM | 0 | 5 | 82 | 2 | 0 | 15 | 79 | 1 | 0 | 1 | 1 | 13 | 0 | 1 | 2 | 7 | 209 | 953 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 6 | 77 | 6 | 0 | 16 | 91 | 2 | 0 | 1 | 1 | 21 | 0 | 1 | 0 | 6 | 228 | 1,005 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 4 | 96 | 5 | 0 | 14 | 87 | 4 | 0 | 6 | 1 | 18 | 0 | 3 | 3 | 9 | 250 | 1,069 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 5 | 97 | 4 | 0 | 12 | 112 | 1 | 0 | 4 | 3 | 15 | 0 | 4 | 1 | 8 | 266 | 1,065 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 6 | 104 | 2 | 0 | 26 | 99 | 1 | 0 | 2 | 0 | 15 | 0 | 1 | 0 | 5 | 261 | 1,068 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 4 | 122 | 6 | 0 | 13 | 111 | 5 | 0 | 5 | 2 | 17 | 0 | 0 | 2 | 5 | 292 | 1,071 | 0 | 0 | 0 | 0 |
| 12:15 PM | 0 | 5 | 104 | 7 | 0 | 15 | 90 | 4 | 0 | 4 | 0 | 9 | 0 | 3 | 1 | 4 | 246 | 1,070 | 0 | 0 | 0 | 0 |
| 12:30 PM | 0 | 3 | 109 | 5 | 0 | 22 | 94 | 2 | 0 | 7 | 3 | 11 | 0 | 2 | 2 | 9 | 269 | 1,083 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 4 | 98 | 2 | 0 | 19 | 110 | 3 | 0 | 2 | 3 | 21 | 0 | 0 | 0 | 2 | 264 | 1,107 | 0 | 0 | 0 | 0 |
| 1:00 PM | 0 | 2 | 113 | 5 | 0 | 31 | 99 | 4 | 0 | 2 | 2 | 27 | 0 | 1 | 0 | 5 | 291 | 1,136 | 0 | 0 | 0 | 0 |
| 1:15 PM | 0 | 3 | 99 | 2 | 0 | 24 | 95 | 3 | 0 | 1 | 1 | 23 | 0 | 2 | 1 | 5 | 259 | 1,146 | 0 | 0 | 0 | 0 |
| 1:30 PM | 0 | 7 | 96 | 6 | 0 | 30 | 113 | 2 | 0 | 5 | 2 | 22 | 0 | 2 | 7 | 1 | 293 | 1,207 | 0 | 0 | 0 | 0 |
| 1:45 PM | 0 | 7 | 102 | 3 | 0 | 37 | 102 | 3 | 0 | 2 | 4 | 16 | 0 | 2 | 8 | 7 | 293 | 1,251 | 0 | 0 | 0 | 0 |
| 2:00 PM | 0 | 5 | 92 | 2 | 0 | 19 | 114 | 1 | 0 | 1 | 9 | 47 | 0 | 2 | 3 | 6 | 301 | 1,284 | 0 | 0 | 0 | 0 |
| 2:15 PM | 0 | 7 | 120 | 5 | 0 | 30 | 117 | 3 | 0 | 2 | 5 | 25 | 0 | 1 | 0 | 5 | 320 | 1,480 | 0 | 0 | 0 | 0 |
| 2:30 PM | 0 | 9 | 125 | 5 | 0 | 22 | 136 | 7 | 0 | 0 | 2 | 20 | 0 | 3 | 3 | 5 | 337 | 1,520 | 0 | 0 | 0 | 0 |


| 2:45 PM | 0 | 9 | 94 | 5 | 0 | 35 | 138 | 3 | 0 | 3 | 1 | 22 | 0 | 2 | 7 | 7 | 326 | 1,605 | 0 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3:00 PM | 0 | 5 | 195 | 3 | 0 | 28 | 142 | 4 | 0 | 9 | 3 | 84 | 0 | 1 | 0 | 23 | 497 | 1,641 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 5 | 148 | 2 | 0 | 34 | 120 | 5 | 0 | 0 | 4 | 30 | 0 | 1 | 4 | 7 | 360 | 1,575 | 0 | 0 | 0 | 0 |
| 3:30 PM | 0 | 4 | 160 | 5 | 0 | 41 | 148 | 6 | 0 | 1 | 6 | 38 | 0 | 1 | 1 | 11 | 422 | 1,529 | 0 | 0 | 0 | 0 |
| 3:45 PM | 0 | 1 | 114 | 1 | 0 | 33 | 155 | 5 | 0 | 1 | 3 | 28 | 0 | 5 | 1 | 15 | 362 | 1,508 | 0 | 0 | 0 | 0 |
| 4:00 PM | 0 | 1 | 141 | 6 | 0 | 44 | 185 | 6 | 0 | 1 | 5 | 23 | 0 | 1 | 0 | 18 | 431 | 1,502 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 1 | 92 | 3 | 0 | 29 | 154 | 3 | 0 | 1 | 2 | 22 | 0 | 1 | 0 | 6 | 314 | 1,713 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 6 | 169 | 2 | 0 | 43 | 124 | 2 | 0 | 1 | 4 | 35 | 0 | 2 | 3 | 10 | 401 | 1,808 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 2 | 130 | 2 | 0 | 22 | 154 | 1 | 0 | 2 | 1 | 28 | 0 | 0 | 0 | 14 | 356 | 1,837 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 4 | 236 | 7 | 0 | 49 | 262 | 8 | 0 | 1 | 1 | 32 | 0 | 3 | 0 | 39 | 642 | 1,804 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 4 | 124 | 4 | 0 | 39 | 177 | 1 | 0 | 3 | 1 | 32 | 0 | 1 | 7 | 16 | 409 |  | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 2 | 152 | 2 | 0 | 34 | 170 | 3 | 0 | 2 | 3 | 46 | 0 | 3 | 4 | 9 | 430 |  | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 119 | 3 | 0 | 23 | 139 | 4 | 0 | 2 | 0 | 24 | 0 | 3 | 2 | 4 | 323 |  | 0 | 0 | 0 | 0 |

## Peak Rolling Hour Flow Rates

| Vehicle Type | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |
| Articulated Trucks | 0 | 4 | 50 | 0 | 0 | 0 | 52 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 111 |
| Lights | 0 | 75 | 757 | 12 | 0 | 122 | 770 | 31 | 0 | 10 | 11 | 153 | 1 | 7 | 1 | 16 | 1,966 |
| Mediums | 0 | 0 | 32 | 0 | 0 | 7 | 26 | 1 | 0 | 1 | 0 | 11 | 0 | 0 | 0 | 0 | 78 |
| Total | 0 | 79 | 839 | 12 | 0 | 129 | 848 | 32 | 0 | 12 | 11 | 164 | 1 | 7 | 1 | 20 | 2,155 |

## Appendix E: Existing Intersection Operational Analysis

## Existing Condition 2019

4: Old Dixie Rd/5 Springs Rd \& SR 3 Performance by run number

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.8 | 0.7 | 0.8 | 0.8 | 0.7 | 0.7 |
| Total Del/Veh (s) | 6.9 | 6.7 | 7.2 | 5.5 | 5.4 | 6.4 |


|  | 4 | $\rightarrow$ | $\geqslant$ | 7 |  | 4 | 4 | $\dagger$ | \％ | ， | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | 「 | ${ }^{7}$ | 中4 | 「 |  | $\uparrow$ | 「 |  | $\uparrow$ | 「 |
| Traffic Volume（veh／h） | 79 | 839 | 12 | 129 | 848 | 32 | 12 | 11 | 164 | 7 | 1 | 20 |
| Future Volume（Veh／h） | 79 | 839 | 12 | 129 | 848 | 32 | 12 | 11 | 164 | 7 | 1 | 20 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 86 | 912 | 13 | 140 | 922 | 35 | 13 | 12 | 178 | 8 | 1 | 22 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（ft） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ft／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  | 2 |  |  | 2 |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal（ft） |  |  |  |  |  |  |  |  |  |  |  |  |
| pX，platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC ，conflicting volume | 922 |  |  | 912 |  |  | 1826 | 2286 | 456 | 1836 | 2286 | 461 |
| $\mathrm{vC1}$ ，stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $v C 2$ ，stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 922 |  |  | 912 |  |  | 1826 | 2286 | 456 | 1836 | 2286 | 461 |
| tC，single（s） | 4.3 |  |  | 4.3 |  |  | 7.7 | 6.7 | 7.1 | 7.7 | 6.7 | 7.1 |
| tC， 2 stage（s） |  |  |  |  |  |  |  |  |  |  |  |  |
| tF（s） | 2.3 |  |  | 2.3 |  |  | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free \％ | 88 |  |  | 80 |  |  | 58 | 51 | 66 | 42 | 96 | 96 |
| cM capacity（veh／h） | 689 |  |  | 695 |  |  | 31 | 24 | 530 | 14 | 24 | 526 |
| Direction，Lane \＃ | EB 1 | EB 2 | EB 3 | EB 4 | WB 1 | WB 2 | WB 3 | WB 4 | NB 1 | SB 1 |  |  |
| Volume Total | 86 | 456 | 456 | 13 | 140 | 461 | 461 | 35 | 203 | 31 |  |  |
| Volume Left | 86 | 0 | 0 | 0 | 140 | 0 | 0 | 0 | 13 | 8 |  |  |
| Volume Right | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 35 | 178 | 22 |  |  |
| cSH | 689 | 1700 | 1700 | 1700 | 695 | 1700 | 1700 | 1700 | 206 | 52 |  |  |
| Volume to Capacity | 0.12 | 0.27 | 0.27 | 0.01 | 0.20 | 0.27 | 0.27 | 0.02 | 0.98 | 0.60 |  |  |
| Queue Length 95th（ft） | 11 | 0 | 0 | 0 | 19 | 0 | 0 | 0 | 213 | 59 |  |  |
| Control Delay（s） | 11.0 | 0.0 | 0.0 | 0.0 | 11.5 | 0.0 | 0.0 | 0.0 | 107.0 | 131.8 |  |  |
| Lane LOS | B |  |  |  | B |  |  |  | F | F |  |  |
| Approach Delay（s） | 0.9 |  |  |  | 1.5 |  |  |  | 107.0 | 131.8 |  |  |
| Approach LOS |  |  |  |  |  |  |  |  | F | F |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 12.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 48．2\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

4: Old Dixie Rd/5 Springs Rd \& SR 3 Performance by run number

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.8 | 0.9 | 0.8 | 0.9 | 0.8 | 0.9 |
| Total Del/Veh (s) | 4.4 | 4.6 | 3.8 | 3.9 | 3.5 | 4.1 |


|  | 4 | $\rightarrow$ |  | 1 | － |  |  | $\uparrow$ | 7 | ＊ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个个 | F | ${ }^{7}$ | 性 | 「 |  | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume（veh／h） | 12 | 642 | 18 | 144 | 763 | 13 | 8 |  | 138 | 7 | 11 | 78 |
| Future Volume（Veh／h） | 12 | 642 | 18 | 144 | 763 | 13 | 8 | 6 | 138 | 7 | 11 | 78 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 13 | 698 | 20 | 157 | 829 | 14 | 9 | 7 | 150 | 8 | 12 | 85 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（ft） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ft／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  | 2 |  |  | 2 |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal（ft） |  |  |  |  |  |  |  |  |  |  |  |  |
| pX，platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC ，conflicting volume | 829 |  |  | 698 |  |  | 1458 | 1867 | 349 | 1522 | 1867 | 414 |
| vC1，stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 829 |  |  | 698 |  |  | 1458 | 1867 | 349 | 1522 | 1867 | 414 |
| tC ，single（s） | 4.3 |  |  | 4.3 |  |  | 7.7 | 6.7 | 7.1 | 7.7 | 6.7 | 7.1 |
| $\mathrm{tC}, 2$ stage（s） |  |  |  |  |  |  |  |  |  |  |  |  |
| tF（s） | 2.3 |  |  | 2.3 |  |  | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free \％ | 98 |  |  | 81 |  |  | 82 | 87 | 76 | 82 | 77 | 85 |
| cM capacity（veh／h） | 749 |  |  | 843 |  |  | 50 | 52 | 624 | 44 | 52 | 565 |
| Direction，Lane \＃ | EB 1 | EB 2 | EB 3 | EB 4 | WB 1 | WB 2 | WB 3 | WB 4 | NB 1 | SB 1 |  |  |
| Volume Total | 13 | 349 | 349 | 20 | 157 | 414 | 414 | 14 | 166 | 105 |  |  |
| Volume Left | 13 | 0 | 0 | 0 | 157 | 0 | 0 | 0 | 9 | 8 |  |  |
| Volume Right | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 14 | 150 | 85 |  |  |
| cSH | 749 | 1700 | 1700 | 1700 | 843 | 1700 | 1700 | 1700 | 530 | 257 |  |  |
| Volume to Capacity | 0.02 | 0.21 | 0.21 | 0.01 | 0.19 | 0.24 | 0.24 | 0.01 | 0.31 | 0.41 |  |  |
| Queue Length 95th（ft） | 1 | 0 | 0 | 0 | 17 | 0 | 0 | 0 | 33 | 47 |  |  |
| Control Delay（s） | 9.9 | 0.0 | 0.0 | 0.0 | 10.2 | 0.0 | 0.0 | 0.0 | 21.5 | 33.4 |  |  |
| Lane LOS | A |  |  |  | B |  |  |  | C | D |  |  |
| Approach Delay（s） | 0.2 |  |  |  | 1.6 |  |  |  | 21.5 | 33.4 |  |  |
| Approach LOS |  |  |  |  |  |  |  |  | C | D |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 4.4 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 43．1\％ |  | CU Level | f Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

No Build Condition
2024 \& 2044

4: Old Dixie Rd/5 Springs Rd \& SR 3 Performance by run number

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 64.3 | 12.0 | 18.9 | 0.8 | 0.7 | 19.3 |
| Total Del/Veh (s) | 33.0 | 26.6 | 43.2 | 7.9 | 6.7 | 23.4 |


|  | $y$ | $\rightarrow$ | 7 | 7 |  | 4 | 4 | 4 | $p$ | ( | $\frac{1}{\dagger}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | T | ${ }^{*}$ | 44 | 「 |  | $\uparrow$ | T |  | $\uparrow$ | 7 |
| Traffic Volume (veh/h) | 85 | 925 | 15 | 140 | 935 | 35 | 15 | 10 | 180 | 5 | 1 | 20 |
| Future Volume (Veh/h) | 85 | 925 | 15 | 140 | 935 | 35 | 15 | 10 | 180 | 5 | 1 | 20 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 92 | 1005 | 16 | 152 | 1016 | 38 | 16 | 11 | 196 | 5 | 1 | 22 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  | 2 |  |  | 2 |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 1016 |  |  | 1005 |  |  | 2002 | 2509 | 502 | 2012 | 2509 | 508 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1016 |  |  | 1005 |  |  | 2002 | 2509 | 502 | 2012 | 2509 | 508 |
| tC , single (s) | 4.3 |  |  | 4.3 |  |  | 7.7 | 6.7 | 7.1 | 7.7 | 6.7 | 7.1 |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 2.3 |  |  | 2.3 |  |  | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free \% | 85 |  |  | 76 |  |  | 25 | 32 | 60 | 24 | 94 | 96 |
| cM capacity (veh/h) | 632 |  |  | 639 |  |  | 21 | 16 | 494 | 7 | 16 | 489 |
| Direction, Lane \# | EB 1 | EB 2 | EB 3 | EB 4 | WB 1 | WB 2 | WB 3 | WB 4 | NB 1 | SB 1 |  |  |
| Volume Total | 92 | 502 | 502 | 16 | 152 | 508 | 508 | 38 | 223 | 28 |  |  |
| Volume Left | 92 | 0 | 0 | 0 | 152 | 0 | 0 | 0 | 16 | 5 |  |  |
| Volume Right | 0 | 0 | 0 | 16 | 0 | 0 | 0 | 38 | 196 | 22 |  |  |
| cSH | 632 | 1700 | 1700 | 1700 | 639 | 1700 | 1700 | 1700 | 134 | 38 |  |  |
| Volume to Capacity | 0.15 | 0.30 | 0.30 | 0.01 | 0.24 | 0.30 | 0.30 | 0.02 | 1.66 | 0.73 |  |  |
| Queue Length 95th (ft) | 13 | 0 | 0 | 0 | 23 | 0 | 0 | 0 | 406 | 67 |  |  |
| Control Delay (s) | 11.7 | 0.0 | 0.0 | 0.0 | 12.4 | 0.0 | 0.0 | 0.0 | 384.8 | 175.3 |  |  |
| Lane LOS | B |  |  |  | B |  |  |  | F | F |  |  |
| Approach Delay (s) | 1.0 |  |  |  | 1.6 |  |  |  | 384.8 | 175.3 |  |  |
| Approach LOS |  |  |  |  |  |  |  |  | F | F |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 36.4 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 51.3\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

4: Old Dixie Rd/5 Springs Rd \& SR 3 Performance by run number

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.8 | 0.9 | 0.9 | 0.8 | 0.8 | 0.8 |
| Total Del/Veh (s) | 4.5 | 6.6 | 4.5 | 4.2 | 4.2 | 4.8 |


|  | 4 | $\rightarrow$ |  | 1 | － |  | 4 | $\uparrow$ | 7 | ， | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个 4 | 「 | ${ }^{7}$ | 性 | 「 |  | $\uparrow$ | 「 |  | $\uparrow$ | F |
| Traffic Volume（veh／h） | 15 | 710 | 20 | 160 | 840 | 15 | 10 | 5 | 150 | 5 | 10 | 85 |
| Future Volume（Veh／h） | 15 | 710 | 20 | 160 | 840 | 15 | 10 | 5 | 150 | 5 | 10 | 85 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 16 | 772 | 22 | 174 | 913 | 16 | 11 | 5 | 163 | 5 | 11 | 92 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（ft） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（tt／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  | 2 |  |  | 2 |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal（ft） |  |  |  |  |  |  |  |  |  |  |  |  |
| pX，platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC ，conflicting volume | 913 |  |  | 772 |  |  | 1614 | 2065 | 386 | 1682 | 2065 | 456 |
| vC1，stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2，stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 913 |  |  | 772 |  |  | 1614 | 2065 | 386 | 1682 | 2065 | 456 |
| tC ，single（s） | 4.3 |  |  | 4.3 |  |  | 7.7 | 6.7 | 7.1 | 7.7 | 6.7 | 7.1 |
| $\mathrm{tC}, 2$ stage（s） |  |  |  |  |  |  |  |  |  |  |  |  |
| tF（s） | 2.3 |  |  | 2.3 |  |  | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free \％ | 98 |  |  | 78 |  |  | 67 | 87 | 72 | 83 | 70 | 83 |
| cM capacity（veh／h） | 694 |  |  | 789 |  |  | 34 | 37 | 590 | 30 | 37 | 530 |
| Direction，Lane \＃ | EB 1 | EB 2 | EB 3 | EB 4 | WB 1 | WB 2 | WB 3 | WB 4 | NB 1 | SB 1 |  |  |
| Volume Total | 16 | 386 | 386 | 22 | 174 | 456 | 456 | 16 | 179 | 108 |  |  |
| Volume Left | 16 | 0 | 0 | 0 | 174 | 0 | 0 | 0 | 11 | 5 |  |  |
| Volume Right | 0 | 0 | 0 | 22 | 0 | 0 | 0 | 16 | 163 | 92 |  |  |
| cSH | 694 | 1700 | 1700 | 1700 | 789 | 1700 | 1700 | 1700 | 388 | 236 |  |  |
| Volume to Capacity | 0.02 | 0.23 | 0.23 | 0.01 | 0.22 | 0.27 | 0.27 | 0.01 | 0.46 | 0.46 |  |  |
| Queue Length 95th（ft） | 2 | 0 | 0 | 0 | 21 | 0 | 0 | 0 | 59 | 55 |  |  |
| Control Delay（s） | 10.3 | 0.0 | 0.0 | 0.0 | 10.9 | 0.0 | 0.0 | 0.0 | 28.1 | 37.3 |  |  |
| Lane LOS | B |  |  |  | B |  |  |  | D | E |  |  |
| Approach Delay（s） | 0.2 |  |  |  | 1.7 |  |  |  | 28.1 | 37.3 |  |  |
| Approach LOS |  |  |  |  |  |  |  |  | D | E |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 5.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 46．0\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

4: Old Dixie Rd/5 Springs Rd \& SR 3 Performance by run number

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 248.9 | 351.5 | 241.2 | 222.4 | 236.2 | 260.8 |
| Total Del/Veh (s) | 62.0 | 170.3 | 159.5 | 63.6 | 73.1 | 105.7 |



4: Old Dixie Rd/5 Springs Rd \& SR 3 Performance by run number

| Run Number | 1 | 2 | 3 | 4 | 5 | Avg |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 234.6 | 281.0 | 294.6 | 148.9 | 216.4 | 235.7 |
| Total Del/Veh (s) | 87.4 | 81.3 | 84.5 | 86.4 | 87.4 | 85.4 |


|  | $\stackrel{ }{*}$ | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ | $p$ | * | $\frac{1}{7}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个 $\uparrow$ | F | \% | ¢4 | 「 |  | $\uparrow$ | F |  | $\uparrow$ | 7 |
| Traffic Volume (veh/h) | 20 | 1055 | 30 | 235 | 1250 | 20 | 15 | 10 | 225 | 10 | 20 | 125 |
| Future Volume (Veh/h) | 20 | 1055 | 30 | 235 | 1250 | 20 | 15 | 10 | 225 | 10 | 20 | 125 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 22 | 1147 | 33 | 255 | 1359 | 22 | 16 | 11 | 245 | 11 | 22 | 136 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (tt/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  | 2 |  |  | 2 |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 1359 |  |  | 1147 |  |  | 2392 | 3060 | 574 | 2492 | 3060 | 680 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1359 |  |  | 1147 |  |  | 2392 | 3060 | 574 | 2492 | 3060 | 680 |
| tC , single (s) | 4.3 |  |  | 4.3 |  |  | 7.7 | 6.7 | 7.1 | 7.7 | 6.7 | 7.1 |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 2.3 |  |  | 2.3 |  |  | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free \% | 95 |  |  | 55 |  |  | 0 | 0 | 45 | 0 | 0 | 64 |
| cM capacity (veh/h) | 462 |  |  | 561 |  |  | 0 | 6 | 443 | 0 | 6 | 376 |
| Direction, Lane \# | EB 1 | EB 2 | EB 3 | EB 4 | WB 1 | WB 2 | WB 3 | WB 4 | NB 1 | SB 1 |  |  |
| Volume Total | 22 | 574 | 574 | 33 | 255 | 680 | 680 | 22 | 272 | 169 |  |  |
| Volume Left | 22 | 0 | 0 | 0 | 255 | 0 | 0 | 0 | 16 | 11 |  |  |
| Volume Right | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 22 | 245 | 136 |  |  |
| cSH | 462 | 1700 | 1700 | 1700 | 561 | 1700 | 1700 | 1700 | 1 | 1 |  |  |
| Volume to Capacity | 0.05 | 0.34 | 0.34 | 0.02 | 0.45 | 0.40 | 0.40 | 0.01 | 366.50 | 228.87 |  |  |
| Queue Length 95th ( ft ) | 4 | 0 | 0 | 0 | 59 | 0 | 0 | 0 | Err | Err |  |  |
| Control Delay (s) | 13.2 | 0.0 | 0.0 | 0.0 | 16.6 | 0.0 | 0.0 | 0.0 | Err | Err |  |  |
| Lane LOS | B |  |  |  | C |  |  |  | F | F |  |  |
| Approach Delay (s) | 0.2 |  |  |  | 2.6 |  |  |  | Err | Err |  |  |
| Approach LOS |  |  |  |  |  |  |  |  | F | F |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1346.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 60.5\% |  | CU Level of | Service |  |  | B |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

## Appendix F: Signal Warrant Analysis

The Worksheet(s) attached are provided as an attachment to the Engineering Investigation Study for:

Intersection: SR 3 @ 5 Springs Rd/Old Dixie Hwy
County: Whitfield
City: Dalton


| Warrant Evaluation Summary | Warrant Met: |
| :---: | :---: |
| Warrant 1: Eight - Hour Vehicular Volume | No |
| Condition A: Minimum Vehicular Volume | No |
| Condition B: Interruption of Continuous Traffic | No |
| Condition C: Combination: $80 \%$ of $A$ and $B$ | No |
| Warrant 2: Four-Hour Volume | No |
| Warrant 3: Peak Hour Volume | No |
| Warrant 4: Pedestrian Volume | N/A |
| Criterion A: Four-Hour |  |
| Criterion B: Peak-Hour |  |
| Warrant 5: School Crossing | N/A |
| Warrant 6: Coordinated Signal System | N/A |
| Warrant 7: Crash Experience | No |
| Warrant 8: Roadway Network | N/A |
| Warrant 9: Intersection Near a Grade Crossing | N/A |

## Warrant Analysis Conducted By:

Name: KB
Agency: Arcadis US Inc.
Date: 4/14/2021


## Warrant Evaluated? Yes Condition justifying use of warrant:

| Criteria |  | Met? |
| :--- | :---: | :---: |
| Delay on Minor Approach | 4 | Yes |
| Volume on Minor Approach | 100 | No |
| Total Entering Volume (veh/h) | 800 |  |

Manually Set Peak Hour?

| Peak Hour | Major Road Vol. <br> (Both App.) | Minor Road Vol. <br> (High App.) |
| :---: | :---: | :---: |
| $7: 00$ | 1895 | 23 |

Warrant Satisfied? No
Manually Set To:

Warrant 4: Pedestrian Volume

Warrant Evaluated? No

Criterion A: Four Hour

| Hour <br> (Start) | Pedestrian <br> Volume | Major <br> Road Vol. |
| :---: | :---: | :---: |
|  |  | 0 |
|  |  | 0 |
|  |  | 0 |
|  |  | 0 |

Manually Set Major Rd Vol?
Avg. walk speed less than $3.5 \mathrm{ft} / \mathrm{s}$ ?

## Criterion A Satisfied?

Criterion B: Peak Hour

| Peak Hour | Pedestrian <br> Vol. | Major <br> Road Vol. |
| :---: | :---: | :---: |
| $0: 00$ | 0 | 0 |

Criterion B Satisfied?

Warrant Satisfied? N/A

Figure 4C-5 Warrant 4, Pedestrian Four-Hour Volume



| 1 | There are a MINIMUM of 20 school children during the highest crossing hour. |  |
| :---: | :--- | :--- |
| 2 | There are fewer adequate gaps in the major road traffic stream during the period when the school children are <br> using the crossing than the number of minutes in the same period. |  |
| 3 | The nearest traffic signal along the major road is located more than 300 ft away. Or, the nearest traffic signal is <br> within 300 ft but the proposed traffic signal will not restrict the progressive movement of traffic. |  |

## Warrant 6: Coordinated Signal System

## Warrant Evaluated? No

Warrant Satisfied? N/A
Manually Set To:
Criteria

|  | Fulfilled? |  |
| :---: | :--- | :--- |
| 1 | Signal spacing > 1000 ft |  |
| 2 | On a one-way road or a road that has traffic predominantly in one direction, the adjacent signals are so far apart <br> that they do not provide the necessary degree of vehicle platooning. |  |
| 3 | On a two-way road, adjacent signals do not provide the necessary degree of platooning and the proposed and <br> the adjacent signals will collectively provide a progressive operation. |  |

Warrant 7: Crash Experience
100\%

## Warrant Evaluated? Yes

Warrant Satisfied? No
Criteria

| Criteria |  |  |  | Met? | Fulfilled? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Adequate trial of other | remedial measures has failed to reduce crash frequend |  |  | Yes |
|  | Measures Tried: |  |  |  |  |
| 2 | Five or more reported crashes, of types susceptible to correction by signal, have occurred within a 12 month period. |  | \# of crashes per 12 months |  | No |
| 2 |  |  | 3 |  |  |
|  | Warrant 1, Condition A | (80\%) |  | No |  |
| 3 | Warrant 1, Condition B | (80\%) |  | No | No |
|  | Warrant 4, Criterion A | (80\%) |  | No |  |
|  | Warrant 4, Criterion B ( | (80\%) |  | No |  |

# Warrant 8: Roadway Network 



## Warrant 9: Intersection Near a Grade Crossing

| Adjustment Factors |  |  | Manually Set Peak Hour? |  |  |  |  | No |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rail Traffic <br> per Day | \% High Occupancy <br> Buses on Minor Road | \% Tractor-Trailer Trucks <br> on Minor Road | D | Peak Hour | Major <br> Road Vol. | Minor <br> Road Vol. | Adjusted <br> Minor Vol. |  |  |  |  |  |
|  |  |  |  | $7: 00$ | 1895 | 23 | 23 |  |  |  |  |  |



[^0]
# Appendix G: Intersection Control Evaluation (ICE) 

| GDOT PI \＃（or N／A）： |  | Request By：GDOT Traffic Ops |
| :---: | :---: | :---: |
| County： | Whitfield | GDOT District： 6 －Cartersville |
| Major（State）Road： | SR 3 | Speed Limit： 55 mph |
| Minor（Crossing）ST： | 5 Springs R | Speed Limit： 50 mph |
| Major ST Direction： | East／West | Area Type：Rural |
| Intersection Control：Conventional（Minor Stop） |  |  |
| Prepared By： | Arcadis | Analyst：Kelli Roberts |
| Date： | 7／15／2020 | Project ID：N／A |
| Safety Improvement |  |  |

2024 Opening Year Volumes

|  |  |  |  |  | 0）［1 |  | 8 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | （0） | （85） | （10） | （5） | क |  |  |  |
|  |  |  | 0 | 20 | 0 | 5 |  |  |  |  |
|  |  | SR 3 | Peds ${ }^{\text {¢ }}$ | $\stackrel{4}{4}$ | $\checkmark$ | $\stackrel{ }{4}$ | $\xrightarrow{\text { Peds }}$ | 0 | （0） | － |
|  | （15） | 85 | 令 | 2024 Intersection Daily Entering Volume（est）： 27，150 |  |  | ${ }_{4}$ | 35 | （15） | 눈 |
|  | （710） | 925 | $\Rightarrow$ |  |  |  | $\Leftarrow$ | 935 | （840） | 응 |
|  | （20） | 15 | $\stackrel{7}{2}$ |  |  |  | ${ }_{5}$ | 140 | （160） | F |
|  | （0） | 0 | $\xrightarrow{\text { Peds }}$ | M | 介 | A | ${ }_{7} 7$ Peds | WB SR 3 |  |  |
|  |  |  | 为 $\square_{0}$ | 15 | 10 | 180 | 0 |  |  |  |
|  |  |  | in | （10） | （5） | （150） | （0） |  |  |  |
|  |  |  | \％ |  | 165） | 100］ |  |  |  |  |



Approach Splits：SR 3－0．88／5 Springs Road－ 0.12

## 2044 Design Year Volumes



Introduction：In 2005，SAFETEA－LU established the Highway Safety Improvement Program（HSIP）and mandated that each state prepare a Strategic Highway Safety Plan（SHSP）to prioritize safety funding investments．Intersections quickly became a common component of most states＇SHSP emphasis areas and HSIP project lists，including Georgia＇s SHSP．Intersection Control Evaluation（ICE）policies and procedures represent a traceable and transparent procedure to streamline the evaluation of intersection control alternatives，and further leverage safety advancements for intersection improvements beyond just the safety program．Approximately one－third of all traffic fatalities and roughly seventy five percent of all traffic crashes in Georgia occur at or adjacent to intersections．Accordingly，the Georgia SHSP includes an emphasis on enhancing intersection safety to advance the Toward Zero Deaths vision embraced by the Georgia Governor＇s Office of Highway Safety（GOHS）．This ICE tool was developed to support the ICE policy，developed and adopted to help ensure that intersection investments across the entire Georgia highway system are selected，prioritized and implemented with defensible benefits for safety towards those ends．

Tool Goal：The goal of this ICE tool is to provide a simplified and consistent way of importing traffic，safety，cost，environmental impact and stakeholder posture data to assess and quantify intersection control improvement benefits．The tool supports the ICE policy and procedures to provide traceability，transparency，consistency and accountability when identifying and selecting an intersection control solution that both meets project purpose and reflects overall best value in terms of specific performance－based criteria．
Requirements：An ICE is required for any intersection improvement（e．g．new or modified intersection，widening／reconstruction or corridor project，or work accomplished through a driveway or encroachment permit that affects an intersection）where：1）the intersection includes at least one roadway designated as a State Route（State Highway System）or as part of the National Highway System；or 2）the intersection will be designed or constructed using State or Federal funding．In certain circumstances where an ICE would otherwise be required，the requirement may be waived based on appropriate evidence presented with a written request．（See the＂Waiver＂tab to review criteria that may make a project waiver eligible and for instructions to submit a waiver request to the Department）．An ICE is not required when the proposed work does not include any changes to the intersection design，involves only routine traffic signal timing and equipment maintenance，or for driveway permits where the driveway is not a new leg to an already existing intersection on either 1）a divided，multi－lane highway with a closed median and only right－in／right－out access or 2 ）an undivided roadway where the development is not required to construct left and／or right turn lanes（as per the Driveway Manual and District Traffic Engineer）．
Two－Stage A complete ICE process consists of two（2）distinct stages，and it is expected that the respective level of effort for completing both stages of ICE will correspond to the Process：magnitude and complexity of the intersection．Prior to starting an ICE，the District Traffic Engineer and／or State Traffic Engineer should be consulted for advice on an appropriate level of effort．The Stage 1 and Stage 2 ICE forms are designed minimize required data inputs using drop－down menu choices and limiting text entry．All fields shaded grey include drop down menu choices and all fields shaded blue require data entry．All other cells in the worksheet are locked．
Stage 1：Stage 1 should be conducted early in the project development process and is intended to inform which altematives are worthy of further evaluation in Stage 2 ．Stage 1 serves Screening as a screening effort meant to eliminate non－competitive options and identify which alternatives merit further considerations based on their practical feasibility．Users should Decision use good engineering judgement in responding to the seven policy questions by selecting＂Yes＂or＂No＂in the drop－down boxes．Alternatives should not be summarily Record eliminated without due consideration，and reasons for eliminating or advancing an alternative should be documented in the＂Screening Decision Justification＂column．
Stage 2：Stage 2 involves a more detailed and familiar evaluation of the altematives identified in Stage 1 in order to support the selection of a preferred altemative that may be advanced
Alternative to detailed design．Stage 2 data entry may require the use of external analysis tools to determine costs，operations and／or safety data that，combined with environmental and
Selection stakeholder posture data，form the basis of the ICE evaluation．A separate＂CostEst＂worksheet tab helps users develop pre－planning－level cost estimates for each Stage 2
Decision alternative evaluated，and a separate Users Guide has been prepared to give guidance on Stage 1 and Stage 2 data entry．Once all data is entered，each alternative is scored
Record and ranked，with the results reported at the bottom of the Stage 2 worksheet to inform on the best of the intersection controls evaluated for project recommendation．
Documentation：A complete ICE document consists of the combination of the outputs from either a completed and signed waiver form or both Stage 1 and Stage 2 worksheets（along with supporting costing and／or environmental documentation），to be included in the approved project Concept Report（or equivalent）or as a stand－alone document．

Geargo Deparmentroftranspatorion

| GDOT PI \# | N/A |
| :--- | :---: |
| Project Location: | SR 3 @ 5 Springs Road |
| Existing Control: | Conventional (Minor Stop) |
| Prepared by: | Arcadis |
| Date: | $7 / 15 / 2020$ |

Note: Up to 5 alternatives may be selected and evaluated; Use this ICE Stage 1 to screen 5 or fewer alternatives to

| Answer "Yes" or "No" to each policy question for |
| :---: |
| each control type to identify which alternatives |
| should be evaluated in the Stage 2 Decision |
| Record; enter justification in the rightmost column | evaluate in Stage 2



GDOT ICE STAGE 2: ALTERNATIVE SELECTION DECISION RECORD

GDOT PI \# (or N/A) N/A County: Whitfield<br>Project Location: SR 3 @ 5 Springs Road<br>Existing Intersection Control: Conventional (Minor Stop)

GDOT District: 6 - Cartersville<br>Area Type: Rural

ICE Version 2.15 | Revised 07/01/2019

Date: 7/15/2020
Agency/Firm: Arcadis Analyst: Kelli Roberts
Type of Analysis: Safety Funded Project

Opening / Design Year Traffic Operations

| Intersection meets signal/AWS warrants? | None |  |
| :--- | :---: | :---: |
| Traffic Analysis Measure of Effectiveness | Intersection Delay |  |
| Traffic Analysis Software Used | Synchro 10 |  |
| Analysis Time Period | AM Peak Hr | PM Peak Hr |
| 2024 Opening Yr No-Build Peak Hr Intersection Delay | 23.4 sec | 4.8 sec |
| 2024 Opening Yr No-Build Peak Hr Intersection V/C | 1.66 | 0.46 |
| 2044 Design Yr No-Build Peak Hr Intersection Delay | 105.7 sec | 85.4 sec |
| 2044 Design Yr No-Build Peak Hr Intersection V/C | 5.00 | 5.00 |
|  |  |  |

Complete Streets Warrants Met?
$\square$ PEDESTRIANS
$\square$ BICYCLES
$\square$ TRANSIT


| Alternatives Analysis: <br> Proposed Control Type/Improvement: <br> Project Cost: (From CostEst Worksheet |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Multilane Roundabout |  | RCUT (stop control) |  | N/A | N/A | N/A |
|  |  |  |  |  |  |  |  |
| Construction Cost | \$1,600,000 |  | \$750,000 |  |  |  |  |
| ROW Cost | \$0 |  | \$50,000 |  |  |  |  |
| Environmental Cost | \$0 |  | \$0 |  |  |  |  |
| Reimbursable Utility Cost | \$100,000 |  | \$50,000 |  |  |  |  |
| Design \& Contingency Cost Cost Adjustment (justification req'd) Total Cost | \$705,000 |  | \$250,000 |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  | \$2,405,000 |  | \$1,100,000 |  |  |  |  |
| Traffic Operations: |  |  |  |  |  |  |  |
| Traffic Analysis Software Used <br> Analysis Period <br> 2044 Design Yr Build Intersection Delay <br> 2044 Design Yr Build Intersection V/C | SIDRA 7 |  | Synchro 10 |  |  |  |  |
|  | AM Peak Hr | PM Peak Hr | AM Peak Hr | PM Peak Hr |  |  |  |
|  | 14.2 sec | 8.8 sec | 4.3 sec | 2.5 sec |  |  |  |
|  | 0.82 | 0.54 | 1.00 | 0.62 |  |  |  |
| Safety Analysis: |  |  |  |  |  |  |  |
| Predefined CRF: PDO <br> Predefined CRF: Fatal/Inj <br> Predefined CRF Source: | 32\% |  | 31\% |  |  |  |  |
|  | 71\% |  | 53\% |  |  |  |  |
|  | FHWA Clearinghouse \#s$236 \text { / } 237$ |  | NC/MO Table 4-7 |  |  |  |  |
| User Defined CRF: PDO | 71\% |  | 43\% |  |  |  |  |
| User Defined CRF: Fatal/Inj | 87\% |  | 54\% |  |  |  |  |
| User Defined CRF Source (write in if applicable): | FHWA Clearinghouse \#s 229 / 230 |  | FHWA Clearinghouse \#s 5556 / 5557 |  |  |  |  |
| Environmental Impacts: ${ }^{1}$ |  |  |  |  |  |  |  |
| Historic District/Property <br> Archaeology Resources <br> Graveyard <br> Stream <br> Underground Tank/Hazmat <br> Park Land <br> EJ Community <br> Wooded Area <br> Wetland | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
|  | None |  | None |  |  |  |  |
| Stakeholder Posture: | Note: If environmental impact is significant ( RED ), provide justification impact won't jeopardize project delivery using "Env" worksheet ${ }^{1}$ Environmental impacts are only preliminary estimates; detailed environmental impact documentation will be included with project concept report |  |  |  |  |  |  |
| Local Community Support GDOT Support | Neutral |  | Neutral |  |  |  |  |
|  | Neutral |  | Neutral |  |  |  |  |
|  |  |  |  |  |  |  |  |
| Final ICE Stage 2 Score: <br> Rank of Control Type Alternatives: | $\begin{gathered} 6.4 \\ 1 \\ \hline \end{gathered}$ |  | $\begin{gathered} 5.6 \\ 2 \\ \hline \end{gathered}$ |  |  |  |  |

Note: Stage 2 score is not given (shown as "-") if signal or AWS is selected as control type but respective warrant are not met
Provide additional comments and/or 2015-2020 Crash Data
explain any unique analysis inputs, or The maximum V/C for the side streets exceeds 5 in the No Build condition results (as necessary): B/C ratio: Multi-lane(13.2) RCUT(16.3)

## Appendix H: Alternatives Operational Analysis

## Build Condition 2044

Multi-lane Roundabout

## LANE SUMMARY

Site: [SR 3 @ 5 Springs/OId Dixie_2044 AM]
New Site
Site Category: (None)
Roundabout
Design Life Analysis (Final Year): Results for 20 years

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{gathered} \text { Lane } \\ \text { Util. } \\ \% \end{gathered}$ | Average Delay sec | Level of Service | 95\% Bac <br> Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: Old Dixie Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 312 | 10.0 | 383 | 0.815 | 100 | 43.9 | LOS E ${ }^{11}$ | 7.8 | 209.6 | Full | 1600 | 0.0 | 0.0 |
| Approach | 312 | 10.0 |  | 0.815 |  | 43.9 | LOS E ${ }^{11}$ | 7.8 | 209.6 |  |  |  |  |
| East: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 763 | 10.0 | 1155 | 0.661 | 100 | 12.3 | LOS B | 6.7 | 181.1 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 926 | 10.0 | 1401 | 0.661 | 100 | 10.7 | LOS B | 7.0 | 187.9 | Full | 1600 | 0.0 | 0.0 |
| Approach | 1689 | 10.0 |  | 0.661 |  | 11.4 | LOS B | 7.0 | 187.9 |  |  |  |  |
| North: 5 Springs Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 40 | 10.0 | 377 | 0.105 | 100 | 11.3 | LOS B | 0.5 | 12.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 40 | 10.0 |  | 0.105 |  | 11.3 | LOS B | 0.5 | 12.8 |  |  |  |  |
| West: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 699 | 10.0 | 1085 | 0.645 | 100 | 12.4 | LOS B | 7.7 | 207.7 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 860 | 10.0 | 1335 | 0.645 | 100 | 10.7 | LOS B | 6.5 | 174.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 1560 | 10.0 |  | 0.645 |  | 11.4 | LOS B | 7.7 | 207.7 |  |  |  |  |
| Intersection | 3600 | 10.0 |  | 0.815 |  | 14.2 | LOS B | 7.8 | 209.6 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.
d Dominant lane on roundabout approach

SIDRA INTERSECTION 8.0 | Copyright © 2000-2019 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: ARCADIS U.S., INC. | Processed: Tuesday, October 19, 2021 11:31:44 AM
Project: C:IUsers\KBoakye\Documents\SR 3 @ 5 Springs Rd.sip8

## LANE LEVEL OF SERVICE

## Lane Level of Service

Site: [SR 3 @ 5 Springs/OId Dixie_2044 AM]
New Site
Site Category: (None)
Roundabout
Design Life Analysis (Final Year): Results for 20 years

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | $\mathrm{E}^{11}$ | B | B | B | B |

11 Level of Service is worse than the Level of Service Target specified in the Parameter Settings dialog.


Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS $F$ will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

## LANE SUMMARY

Site: [SR 3 @ 5 Springs/OId Dixie_2044 PM]
New Site
Site Category: (None)
Roundabout
Design Life Analysis (Final Year): Results for 20 years

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| South: Old Dixie Hwy |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 251 | 10.0 | 541 | 0.464 | 100 | 14.7 | LOS B | 2.7 | 73.4 | Full | 1600 | 0.0 | 0.0 |
| Approach | 251 | 10.0 |  | 0.464 |  | 14.7 | LOS B | 2.7 | 73.4 |  |  |  |  |
| East: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 711 | 10.0 | 1328 | 0.535 | 100 | 8.5 | LOS A | 4.9 | 133.5 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 834 | 10.0 | 1559 | 0.535 | 100 | 7.6 | LOS A | 5.0 | 134.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 1545 | 10.0 |  | 0.535 |  | 8.0 | LOS A | 5.0 | 134.3 |  |  |  |  |
| North: 5 Springs Road |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 152 | 10.0 | 500 | 0.305 | 100 | 11.9 | LOS B | 1.4 | 37.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 152 | 10.0 |  | 0.305 |  | 11.9 | LOS B | 1.4 | 37.2 |  |  |  |  |
| West: SR 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 505 | 10.0 | 1065 | 0.474 | 100 | 8.8 | LOS A | 3.4 | 92.2 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 628 | 10.0 | 1325 | 0.474 | 100 | 7.5 | LOS A | 3.6 | 96.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 1134 | 10.0 |  | 0.474 |  | 8.1 | LOS A | 3.6 | 96.7 |  |  |  |  |
| Intersection | 3082 | 10.0 |  | 0.535 |  | 8.8 | LOS A | 5.0 | 134.3 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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Organisation: ARCADIS U.S., INC. | Processed: Tuesday, October 19, 2021 11:39:05 AM
Project: C:IUsers\KBoakye\Documents\SR 3 @ 5 Springs Rd.sip8

## LANE LEVEL OF SERVICE

## Lane Level of Service

Site: [SR 3 @ 5 Springs/OId Dixie_2044 PM]
New Site
Site Category: (None)
Roundabout
Design Life Analysis (Final Year): Results for 20 years

|  | Approaches |  |  |  | Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | South | East | North | West |  |
| LOS | B | A | B | A | A |



Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS $F$ will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.

## Build Condition 2044

RCUT

4: Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBR | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh $(\mathrm{s})$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.1 | 0.0 |
| Total DelVeh $(\mathrm{s})$ | 14.1 | 1.8 | 1.8 | 20.8 | 1.6 | 2.2 | 13.8 | 1.5 | 4.3 |

## 6: Performance by movement

| Movement | EBU | EBT | WBT | All |
| :--- | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.4 | 0.2 |
| Total Del/Veh (s) | 40.3 | 3.4 | 1.6 | 3.0 |

## 8: Performance by movement

| Movement | EBT | WBU | WBT | All |
| :--- | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.3 | 0.0 | 0.0 | 0.2 |
| Total Del/Veh (s) | 1.4 | 42.1 | 1.4 | 1.5 |

## Total Network Performance

|  |  |
| :--- | ---: |
| Denied Del/Veh (s) | 0.3 |
| Total DelVeh (s) | 10.2 |

4:


4: Performance by movement

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBR | SBR | All |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Denied Del/Veh $(\mathrm{s})$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 | 0.2 | 0.0 |
| Total Del/Veh $(\mathrm{s})$ | 10.5 | 1.3 | 1.9 | 11.2 | 1.4 | 2.0 | 3.6 | 3.6 | 2.5 |

6: Performance by movement

| Movement | EBU | EBT | WBT | All |
| :--- | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.0 | 0.0 | 0.3 | 0.2 |
| Total Del/Veh (s) | 28.2 | 2.4 | 1.4 | 2.1 |

8: Performance by movement

| Movement | EBT | WBU | WBT | All |
| :--- | ---: | ---: | ---: | ---: |
| Denied Del/Veh (s) | 0.2 | 0.0 | 0.0 | 0.1 |
| Total Del/Veh (s) | 1.0 | 29.0 | 2.0 | 1.9 |

## Total Network Performance

|  |  |
| :--- | :--- |
| Denied Del/Veh (s) | 0.3 |
| Total DelVeh (s) | 7.6 |

4:


## Appendix I: Summary of Right-of-way and Construction Costs Estimates

## CONSTRUCTION COST ESTIMATE SR 3 @ 5 Springs Rd/OId Dixie Hwy

| PAY ITEM | DESCRIPTION | UNIT | QUANTITY |  | PRICE | AMOUNT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 150-1000 | TRAFFIC CONTROL - |  | 1 | \$ | 150,000.00 | \$ | 150,000.00 |
| 150-5010 | TRAFFIC CONTROL, PORTABLE IMPACT ATTENUATOR | EA | 4 | \$ | 8,014.30 | \$ | 32,057.22 |
| 210-0100 | GRADING COMPLETE - | LS | 1 | \$ | 200,000.00 | \$ | 200,000.00 |
| 310-1101 | GR AGGR BASE CRS, INCL MATL | TN | 1045 | \$ | 30.49 | \$ | 31,866.07 |
| 402-3121 | RECYCLED ASPH CONC 25 MM SUPERPAVE, GP 1 OR 2, INCL BITUM MATL \& H LIME | TN | 250 | \$ | 85.42 | \$ | 21,354.79 |
| 402-3190 | RECYCLED ASPH CONC 19 MM SUPERPAVE, GP 1 OR 2,INCL BITUM MATL \& H LIME | TN | 100 | \$ | 92.30 | \$ | 9,229.98 |
| 402-3130 | RECYCLED ASPH CONC 12.5 MM SUPERPAVE, GP 2 ONLY, INCL BITUM MATL \& H LIME | TN | 855 | \$ | 108.67 | \$ | 92,909.71 |
| 413-0750 | TACK COAT | GL | 625 | \$ | 2.60 | \$ | 1,626.36 |
| 429-1000 | RUMBLE STRIPS | EA | 12 | \$ | 752.63 | \$ | 9,031.59 |
| 432-0206 | MILL ASPH CONC PVMT, $11 / 2$ IN DEPTH | SY | 9425 | \$ | 4.72 | \$ | 44,477.56 |
| 439-0022 | PLAIN PC CONC PVMT, CL 3 CONC, 10 INCH THK | SY | 536 | \$ | 94.13 | \$ | 50,451.30 |
| 441-0748 | CONCRETE MEDIAN, 6 IN | SY | 1042 | \$ | 66.96 | \$ | 69,776.35 |
| 441-5008 | CONCRETE HEADER CURB, 6 IN, TP 7 | LF | 285 | \$ | 17.28 | \$ | 4,924.09 |
| 441-5025 | CONCRETE HEADER CURB, 4 IN, TP 9 | LF | 405 | \$ | 17.11 | \$ | 6,930.04 |
| 441-6222 | CONC CURB \& GUTTER, 8 IN X 30 IN, TP 2 | LF | 1720 | \$ | 31.00 | \$ | 53,327.94 |
| 446-1100 | PVMT REINF FABRIC STRIPS, TP 2, 18 INCH WIDTH | LF | 1130 | \$ | 5.97 | \$ | 6,744.23 |
| 643-8200 | BARRIER FENCE (ORANGE), 4 FT | LF | 3580 | \$ | 2.15 | \$ | 7,699.70 |
| 550-1180 | STORM DRAIN PIPE, 18 IN, H 1-10 | LF | 900 | \$ | 52.91 | \$ | 47,616.61 |
| 668-1100 | CATCH BASIN, GP 1 | EA | 8 | \$ | 2,709.73 | \$ | 21,677.88 |
| 668-2100 | DROP INLET, GP 1 | EA | 8 | \$ | 2,508.99 | \$ | 20,071.94 |
| 163-0232 | TEMPORARY GRASSING | AC | 1 | \$ | 585.34 | \$ | 585.34 |
| 163-0240 | MULCH | TN | 3 | \$ | 303.10 | \$ | 909.31 |
| 163-0300 | CONSTRUCTION EXIT | EA | 4 | \$ | 1,612.65 | \$ | 6,450.61 |
| 163-0503 | CONSTRUCT AND REMOVE SILT CONTROL GATE, TP 3 | EA | 2 | \$ | 491.01 | \$ | 982.01 |
| 700-6910 | PERMANENT GRASSING | AC | 2 | \$ | 1,240.82 | \$ | 2,481.63 |
| 700-7000 | AGRICULTURAL LIME | TN | 4 | \$ | 129.92 | \$ | 519.67 |
| 700-8000 | FERTILIZER MIXED GRADE | TN | 1 | \$ | 829.36 | \$ | 829.36 |
| 700-8100 | FERTILIZER NITROGEN CONTENT | LB | 200 | \$ | 4.92 | \$ | 984.18 |
| 716-2000 | EROSION CONTROL MATS, SLOPES | SY | 500 | \$ | 1.59 | \$ | 793.96 |
| 636-1033 | HIGHWAY SIGNS, TP 1 MATL, REFL SHEETING, TP 9 | SF | 100 | \$ | 20.42 | \$ | 2,041.84 |
| 636-2080 | GALV STEEL POSTS, TP 8 | LF | 168 | \$ | 10.63 | \$ | 1,785.48 |
| 653-0110 | THERMOPLASTIC PVMT MARKING, ARROW, TP 1 | EA | 2 | \$ | 86.39 | \$ | 172.77 |
| 653-0120 | THERMOPLASTIC PVMT MARKING, ARROW, TP 2 | EA | 2 | \$ | 90.51 | \$ | 181.02 |
| 653-0130 | THERMOPLASTIC PVMT MARKING, ARROW, TP 3 | EA | 4 | \$ | 143.44 | \$ | 573.77 |
| 653-0296 | THERMOPLASTIC PVMT MARKING, WORD, TP 15 | EA | 7 | \$ | 211.19 | \$ | 1,478.32 |
| 653-1501 | THERMOPLASTIC SOLID TRAF STRIPE, 5 IN, WHITE | LF | 5824 | \$ | 1.04 | \$ | 6,040.98 |
| 653-1502 | THERMOPLASTIC SOLID TRAF STRIPE, 5 IN, YELLOW | LF | 3400 | \$ | 0.99 | \$ | 3,360.37 |
| 653-1806 | THERMOPLASTIC SOLID TRAF STRIPE, 8 IN, YELLOW | LF |  | \$ | 2.42 | \$ | - |
| 653-3501 | THERMOPLASTIC SKIP TRAF STRIPE, 5 IN, WHITE | GLF | 1080 | \$ | 11.66 | \$ | 12,588.38 |
| 654-1001 | RAISED PVMT MARKERS TP 1 | EA | 400 | \$ | 5.08 | \$ | 2,031.01 |
| 654-1003 | RAISED PVMT MARKERS TP 3 | EA | 400 | \$ | 5.17 | \$ | 2,069.70 |
| 500-3101 | CLASS A CONCRETE | CY | 0.5 | \$ | 1,125.18 | \$ | 562.59 |
| 511-1000 | BAR REINF STEEL | LB | 2600 | \$ | 1.24 | \$ | 3,216.91 |
| 647-2120 | PULL BOX, PB-2 | EA | 12 | \$ | 495.65 | \$ | 5,947.84 |
| 681-4220 | LIGHTING STD, 40 FT MH, POST TOP | EA | 4 | \$ | 3,625.33 | \$ | 14,501.32 |
| 681-6470 | LUMINAIRE, TP 4, 275 W, LED | EA | 22 | \$ | 932.65 | \$ | 20,518.30 |
| 682-1506 | CABLE, TP RHH/RHW, AWG NO 6 | LF | 1300 | \$ | 1.36 | \$ | 1,765.83 |
| 682-6222 | CONDUIT, NONMETL, TP 2, 2 IN | LF | 1300 | \$ | 9.08 | \$ | 11,804.06 |
| 682-6233 | CONDUIT, NONMETL, TP 3, 2 IN | LF | 1300 | \$ | 6.26 | \$ | 8,135.66 |
| 682-9000 | MAIN SERVICE PICK UP POINT | LS | 1 | \$ | 10,000.00 | \$ | 10,000.00 |
| 682-9010 | SVC POLE RISER | EA | 12 | \$ | 2,335.45 | \$ | 28,025.38 |
| 682-9950 | DIRECTIONAL BORE - | LF | 150 | \$ | 15.72 | \$ | 2,358.12 |
| 700-9300 | SOD | SY | 280 | \$ | 8.26 | \$ | 2,312.90 |
| 702-0212 | CRATAEGUS VIRIDIS - | EA | 3 | \$ | 631.89 | \$ | 1,895.67 |
| 702-0470 | ILEX VOMITORIA NANA - | EA | 100 | \$ | 53.62 | \$ | 5,361.68 |
| 702-9005 | SPRING APPLICATION FERTILIZER | LB | 100 | \$ | 11.59 | \$ | 1,159.48 |
| 702-9025 | LANDSCAPE MULCH | SY | 280 | \$ | 9.99 | \$ | 2,797.34 |
|  |  |  | GINEERING | D I | ECTION | \$ | 1,048,996.17 |
|  |  |  |  | CO | NGENCY | \$ | 104,899.62 |
|  |  |  |  |  | (rounded) | \$ | 1,154,000.00 |

## Appendix I: Safety Benefit-Cost Analysis




## Appendix K: Environmental Screening Report

GDOT Office of Traffic Operations<br>935 Confederate Ave., SE<br>Atlanta, GA 30316<br>Subject: Environmental Screening Memo<br>State Route (SR) 3 @ Five Springs Road/Old Dixie Highway<br>Arcadis U.S., Inc.<br>2410 Paces Ferry Road<br>\#400<br>Atlanta<br>Georgia 30339<br>Tel 7704318666<br>Fax 7704352666 P.I. No. N/A, Whitfield Co., Georgia

The Georgia Department of Transportation (GDOT) has identified the need for improvements to State Route (SR) 3 @ Five Springs Road/Old Dixie Highway, in Whitfield County, Georgia. The proposed project is to be included in the GDOT Safety Lump Sum Program within the Office of Traffic Operations.
SR 3 is a four-lane rural major arterial that runs in the east-west direction with a posted speed limit of 55 miles per hour (MPH). Old Dixie Highway is a two-lane rural major collector that connects traffic from the south to the intersection. The posted speed limit along Old Dixie Hwy is 50 MPH. Five Springs Rd is a twolane rural local road that connects traffic from the north to the intersection. The posted speed limit along Five Springs Rd is 40 MPH . The intersection is stop controlled on the side streets (Five Springs Rd/Old Dixie Hwy).

The proposed project is the conversion of a four (4) legged, two-way stop-controlled intersection, to a Multi Lane Roundabout (MLR). The roundabout would maintain the 4 approaches with adjustments to include the required horizontal curves/radii to slow the traffic prior to entering the circulatory roadway. The proposed roundabout may require additional Right-of-Way (ROW); however, the project's development is in early stages and specific related information is yet to be determined.

To assist GDOT in understanding the potential environmental constraints within the corridor, Arcadis staff conducted a desktop survey. Arcadis used National Wetland Inventory (NWI) maps, Georgia's Natural, Archaeological, and Historic Geographic Information System (GNAHRGIS), the U.S. Environmental Protection Agency's (USEPA) EnviroMapper, and the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps (FIRM) to identify environmental resources that may be afforded protection under the National Environmental Policy Act (NEPA). Based on the desktop survey, the following environmental concerns/constraints were observed in the corridor:

## NEPA

## Environmental Justice/Community Impact

During this desktop survey, the presence of minority or low-income populations was not apparent within the study corridor. The nature of the proposed project (converting an existing intersection into a roundabout) is minor and is unlikely to result in disproportionate effects to minority or low-income residents.

## Section 4(f) Properties

Section 4(f) properties include significant publicly owned public parks, recreation areas, and wildlife or waterfowl refuges, or any publicly or privately owned historic site listed or eligible for listing on the National Register of Historic Places (NRHP). Historic properties that may be afforded protection under Section 4(f) were identified within and adjacent to the project limits. Please see the History discussion on page 4 of this screening for more information.

## Environmental Documentation

Based on the 2018 Programmatic Categorial Exclusion (PCE) Process Agreement, the proposed project type is minor and may qualify for a PCE; however, for planning purposes it is assumed that environmental clearance will be obtained with a CE.

## Ecology

## Protected Species

The proposed SR 3 @ Five Springs Road/Old Dixie Highway project is approximately 4.18 miles south of Dalton, GA. Protected species and their habitats may exist but are less likely to exist within the project corridor due to development, utility easements and proximity to the existing roadway. A separate discussion regarding bat species follows. An Ecological Resource Survey Report and Assessment of Effects for protected species and their habitats would be prepared to assess habitat suitability, species presence, and the effect of the proposed project on protected species.

Bats
All bats are protected under Georgia state law and some species have additional protections under the federal Endangered Species Act of 1973. Bridges and culverts are often potential bat roosting locations and forested areas can serve as roosting and foraging habitat. The proposed project is adjacent to forested areas within the range of the Gray Bat (Myotis grisescens). The United States Fish \& Wildlife Service's Interim Guidance: Bat Consultation Ranges (October 7, 2019) showed no additional species for the area.

## Waters of the United States

According to the NWI map, there are Waters of the United States near the study corridor (Figure 1). None of these waters are designated as trout streams. An Ecological Resource Survey would be necessary to confirm the extent of any jurisdictional and state waters within the project corridor. Additionally, an Assessment of Effects would be necessary to analyze and document the impacts of the project on jurisdictional and state waters should any be confirmed.

Figure 1. Waters of the United States


## Floodplain

FEMA FIRM Panel 13313CO230D, Whitfield County (dated 09/09/2007) was reviewed to identify flood hazard zones within the project corridor. Based on this review, a portion of the study corridor contains a flood zone or flood hazard area (Figure 2). Coordination with project engineers and designers is necessary to confirm the location of the floodplain and any impacts resulting from the proposed project's design. Encroachments and fill impacts within the Zone AE floodplain and regulatory floodway would necessitate a hydraulic study to be conducted to measure the resulting increases in floodplain and floodway elevations and floodway width. Efforts to avoid and minimize fill impacts will be undertaken as design and plan development proceed.

Figure 2. Floodplain


## History

A GNAHRGIS query returned one (1) result for historic resources (structures 50 years of age and older) within or adjacent to the project corridor. Five (5) historic resources were identified using information from the Whitfield County Tax Assessor. These resources are listed below (Figure 3). Note: this segment of Old Dixie Highway may be determined to be eligible for listing in the National Register of Historic Places (NRHP). Section 106 Coordination and a Historic Resources Survey Report by a certified historian would be necessary to confirm the full extent of historic resources and their eligibility for listing in the NRHP. Preparation of a Cultural Resources Assessment of Effects Report may be necessary.
A. 3092 Five Springs Rd, 1961
B. 3072 Five Springs Rd, 1961
C. 3051 Five Springs Rd, 1961 (GNAHRGIS data point)
D. 3067 Five Springs Rd, 1961
E. 3073 Five Springs Rd, 1961

Figure 3. Historic Resources


## Archaeology

According to GNAHRGIS, no publicly documented archaeological resources are present within the project limits, and the possibility of encountering archaeological resources is low. Most of the areas adjacent to the study corridor have been modified and disturbed by transportation facilities, utilities, and other development. Based on the desktop survey, Section 106 Coordination and an Archaeological Short Report appears to be the likely path for reporting; a site file search and field work by certified archaeologists may necessitate the preparation of a Management Summary and a Phase 1 Archaeology Resource Report if previously listed sites or newly uncovered sites are confirmed or found.

## Hazardous Waste/Underground Storage Tanks

The EPA's EnviroMapper, Georgia Environmental Protection Division's (GAEPD) underground storage tank (UST) database, and desktop surveys, were used to identify facilities with UST(s) that are present within the study corridor. None were found. Should unpredicted UST(s) be located, a Phase I Environmental Site Assessment (ESA) would likely be necessary, and a Phase II ESA could be required.

## Public Involvement

A determination on the level of public involvement has not yet been made. A Public Information Open House (PIOH) may be recommended.

## Anticipated Permits

No permits are anticipated. A U.S. Army Corps of Engineers (USACE) Section 404 Permit would be required if impacts to Waters of the U.S. were unavoidable.

## Appendix L: Existing and Preferred Alternative Sketches




## Appendix M: Roundabout Checks and Layout Iterations










## Appendix N: Previous GDOT TE Study (4/20/2020)

## GDYT <br> Georgia Department of Transportation



SR 3 @ Old Dixie HWY/ Five Springs Rd Whitfield County

04/20/2020
Prepared By: Manara ALI

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## STUDY LOCATION

The location of study is at intersection SR 3 @ Old Dixie HWY/ Five Springs Rd in Whitfield County.

## REASON FOR INVESTIGATION

The intersection of SR 3 @ Old Dixie Hwy/ Five Springs Rd is being analyzed due to a fatality and different safety and operation concerns.

## TOPOGRAPHY

The studied intersection, SR 3 @ Old Dixie Hwy/ Five Springs Rd, is a relatively flat intersection in urbanized area. Direction of travel for SR 3 is East/West with this section of road composed of fourlanes Urban Arterial. State Route SR 3 currently is a four-lane, 13-foot-wide undivided highway with unpaved, grass shoulders. The speed limit along State Route SR 3 is posted as 55 MPH . The intersecting roads, Five Springs Rd and Old Dixie Hwy are Rural Major Collector roads with a North/South direction of travel, respectively. The intersecting roads are both two-lane undivided with grass shoulder roadway with a speed limit of 50 MPH for Old Dixie Hwy and 40 MPH for Five Springs Rd. This intersection is considered an Urban area.
The required sight distance for Old Dixie Hwy/ Five Springs Rd at the intersection with SR 3, based on the Regulation for Driveway and Encroachment Control Manual is 690 feet for traffic approaching the minor road from the left and 610 feet for traffic approaching the side road from the right. Upon site visit at the intersection of SR 3 and Old Dixie Hwy/ Five Springs Rd, sight distances were measured and recorded as presented in the table below.

|  | Sight Distance on <br> Old Dixie Hwy/ Five Springs Rd <br> (Feet) |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | SDL | SDR | SDL | Sive Springs Rd |
|  | 690 | 610 | 690 | 610 |
| Required <br> Sight distance | 1600 | 1830 | 1830 | 1600 |
| Measured <br> Sight Distance |  |  |  |  |

**All measurements where determined based on Regulation for Driveway and Encroachment Control Manual for a 55 MPH speed limit on the mainline SR 3.

## EXISTING TRAFFIC CONTROL

The current existing traffic control is Two-Way stop controlled at this intersection. The main line, SR 3, is free flow, while the side roads, Old Dixie Hwy and Five Springs Rd are stop controlled.

## VEHICLE VOLUME HISTORY

The AADT for State Route SR 3 is 10,600 with a $6 \%$ Truck and Old Dixie Hwy/ Five Springs volume is 2,010 from the Transportation Data Viewer. A 12-hour traffic count was collected at the above intersection and data tabulated in Appendix H.

## PEDESTRIAN MOVEMENTS

## None Observed.

## CRASH HISTORY

Crash reports were generated through the GEARS Database over a study period of five (5) years. There has been a total of 28 crashes between January 1st 2015 and April 20 ${ }^{\text {th }}, 2020$. From these collected data, the crash data distribution read as follows, 16 Angle crashes and 11 Rear End and 1 Side-swipe crashes collision.
The crash data was distributed as follows:

- 7 Angle crashes originated from Old Dixie Hwy, out of which 6 were Right Angle crashes between commuters attempting to cross SR 3 coming off Old Dixie Hwy and crashing with both Eastbound and Westbound traffic, 1 Left turn angle crash between commuters attempting to turn and left onto SR 3 coming off Old Dixie Hwy and crashing with Eastbound traffic. 6 Angle crashes originated from SR 3, out of which 5 were Left turn angle crashes between commuters attempting to turn left onto Old Dixie Hwy coming off the main line SR 3 and crashing with Eastbound traffic and 1 Left turn angle crash between commuters attempting to turn left onto Five Springs Rd coming off the main line SR 3 and crashing with Westbound traffic.
3 Angle crashes originated from Five Springs Rd, out of which 2 were Right angle crashes between commuters attempting to cross SR 3 and crashing with both Eastbound and Westbound traffic and 1 Left turn angle crash between commuters attempting to turn left onto SR 3 coming off the main line Five Springs Rd and crashing with Northbound traffic.
- 11 Rear End crashes on Old Dixie Hwy, all of which were between Northbound commuters.
- 1 Side-swipe crash between Southbound commuters on Five Springs Rd.

| SR 3 @ Old Dixie Hwy/ Five Springs Rd |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | $\mathbf{2 0 1 5}$ | $\mathbf{2 0 1 6}$ | $\mathbf{2 0 1 7}$ | $\mathbf{2 0 1 8}$ | $\mathbf{2 0 1 9}$ | $\mathbf{2 0 2 0}$ | Total per Crash Type |  |
| Angle | 3 | 1 | 1 | 4 | 7 | 0 | 16 |  |
| Head On | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Rear End | 2 | 0 | 2 | 2 | 4 | 1 | 11 |  |
| Side Swipe | 1 | 0 | 0 | 0 | 0 | 0 | 1 |  |
| Total per Year | 6 | 1 | 3 | 6 | 11 | 1 | $\mathbf{7}$ |  |
| Grand Total |  |  |  |  |  |  |  |  |
| Injuries | 3 | 0 | 0 | 5 | 4 | 0 | $\mathbf{2 8}$ |  |
| Fatalities | 0 | 0 | 0 | 0 | 0 | 1 | $\mathbf{1 2}$ |  |

## ADJACENT SIGNALIZED INTERSECTIONS

The nearest traffic signal is within 1,800 feet in the Eastbound direction of the intersection.

## SPEED STUDY

The posted speed limit on State Route SR 3 within the study area is 55 MPH , which is enforceable through radar surveillance by the Whitfield County Sheriff's Office and the Department of Public Safety.

## ROUNDABOUT ANALYSIS

The total volumes for the intersection are 12,610 with volumes on State Route SR 3 equivalent to 10,600 and contribution from Old Dixie Hwy/ Five Springs Rd equivalent to 2,010 vehicles. These contributions are equivalent to $84 \%$ of the total volumes for SR 3 and $16 \%$ of total volumes for Old Dixie Hwy/ Five Springs Rd. Because the contribution from the minor road, Old Dixie Hwy/ Five Springs Rd, is over $10 \%$ of the total volumes, a roundabout intersection as an alternative intersection design is considered in our study and results of the study are summarized below and full report in Appendix C.

| SR 3 @ Old Dixie Hwy/ Five Springs Rd |  |
| :---: | :---: |
| Approach Delays <br> (s/veh) | 10.7 |
| Level of Service | B |

## MUTCD WARRANT ANALYSIS

Traffic signal warrant analysis was performed for the intersection of State Route SR 3 @ Old Dixie Hwy/ Five Springs Rd using the criteria provided in the Manual on Uniform Traffic Control Device (MUTCD) published by the Federal Highway Administration (FWHA). According to the MUTCD, the investigation of the need for traffic control signal shall include an analysis of the applicable factors contained in the following traffic signal warrants and other factors related to existing operation and safety at the study location:

- Warrant 1 - Eight Hour Volume
- Warrant 2 - Four Hour Volume
- Warrant 3 - Peak Hour
- Warrant 4 - Pedestrian Volume
- Warrant 5 - School Crossing
- Warrant 6 - Coordinated Signal System
- Warrant 7 - Crash Experience
- Warrant 8 - Roadway Network

None of the 8 warrants were satisfied for this intersection.

## HCS7 TWO-WAY STOP CONTROL ANALYSIS

A Two-Way stop control analysis was conducted at the intersection of SR 3 @ Old Dixie Hwy/ Five Springs Rd and a level of service of E and F was returned for both Old Dixie Hwy and Five Springs Rd
respectively. However, analysis of State Route SR 3, direction of travel East/West, resulted in an approach Level of Service of B in either direction during peak hour. Parts of the Two-Way stop control report describing the different Level of Service and approach delays at the intersection of State Route SR 3 @ Old Dixie Hwy/ Five Springs Rd are summarized below, and full report can be found in Appendix E.

|  | Eastbound | Westbound | Northbound | Southbound |
| :---: | :---: | :---: | :---: | :---: |
| Approach Delays <br> (s/veh) | 0.9 | 1.4 | 49.2 | 108.1 |
| Level of Service | B | B | E | F |

## HCS7 ALL WAY STOP CONTROL

An All-Way stop control analysis was conducted at the intersection of SR 3 @ Old Dixie Hwy/ Five Springs Rd and an intersection delay of 73.8 seconds per vehicle and a Level of Service of F was recorded as the overall intersection performance. Based on these results, it is evident that converting the intersection at SR 3 @ Old Dixie Hwy/ Five Springs Rd will translate into a worst overall performance for the intersection especially for commuters traveling the main line SR 3. Although this intersection meets warrants for an All-Way Stop according to the MUTCD Section 2B. 07 criterion C, regarding minimum volumes, it states that vehicular volume entering the intersection from the major street approaches (total of both approaches) in both directions averages at least 300 vehicles per hour for any 8 hours of an average day; AND the combined vehicular, pedestrian, and bicycle volume entering the intersection from the minor street approaches (total of both approaches) averages at least 200 units per hour for the same 8 hours, WITH an average delay to minor-street vehicular traffic of at least 30 seconds per vehicle during the highest hour, we will not consider this alternative as it will not improve operation at the intersection of SR 3 @ Old Dixie Hwy/ Five Springs Rd.
Parts of the All-Way Stop Control report summarizing Level of Service and approach delays at the intersection of State Route SR 3 and Old Dixie Hwy/ Five Springs Rd are recounted below and full report can be found in Appendix F.

| SR 3 @ Old Dixie Hwy/ Five Springs Rd |  |
| :---: | :---: |
| Intersection Delays <br> (s/veh) | 73.8 |
| Level of Service | F |

## HCS7 TWO-WAY STOP CONTROL RCUT ANALYSIS

Finally, a Two-Way stop controlled Restricted Crossing U-Turn or RCUT intersection analysis was performed at the intersection of SR 3 @ Old Dixie Hwy/ Five Springs Rd. This alternative intersection proved to have a higher performance level than all other considered alternatives. In fact, results from the ICE analysis indicated an intersection delay of 2.8 seconds per vehicle with a Level of Service of A for the entire intersection. Parts of the RCUT report summarizing Level of Service and intersection delays at State Route SR 3 @ Old Dixie Hwy/ Five Springs Rd are recounted below, and full report can be found in Appendix G.

| SR 3 @ Old Dixie Hwy/ Five Springs Rd |  |
| :---: | :---: |
| Intersection Delays <br> (s/veh) | 2.8 |
| Level of Service | A |

## CONCLUSION

Considering the various alternatives we looked at, Two-Way stop control (existing condition), All-way stop control, Traffic Signal, Multi-lane Roundabout, RCUT, and Offset Left Turn Lanes the most feasible options were either upgrading the intersection to a Multi-Lane Roundabout, reshaping the intersection as an RCUT intersection or redesigning the current intersection to an Offset left turn lanes intersection. Level of Service, approach delays and safety concerns were analyzed. Due to its high approach delays, poor level of service and the current recorded fatality, the Two-Way stop control made it a less desirable alternative than all other presented alternatives. Based on the Signal Warrant Analysis, a traffic signal is not a recommended feasible alternative to consider in order to improve traffic operation, level of service and safety at the intersection of State Route SR 3 @ Old Dixie Hwy/ Five Springs. GDOT ICE Tool was then used to examine and rank the remaining alternatives, Multilane Roundabout, RCUT and Offset Left Turn Lane. The GDOT tool found the Multi-lane Roundabout to be the most desirable intersection alternative for the intersection of SR 3 @ Old Dixie Hwy/ Five Springs, and report of this ranking can be found in Appendix B

## RECOMMENDATIONS

Our recommendations for this intersection are to convert the existing intersection into a multi-lane roundabout which will address the majority of the crashes found here.

This intersection will be submitted to the statewide safety office for further review and assessment, while District 6 Traffic Operations will continue to monitor this intersection after the additional changes have been made, but also during the statewide safety assessment for the feasibility of a safety project to determine if further measures can be taken.

PREPARED BY: $\qquad$ DATE: $\qquad$ Civil Engineer II

RECOMMENDED BY: $\qquad$ DATE:
District Traffic Engineer

Whitfield Co.

## Frequently Asked Questions:

Question 1: What is new in ICE Version 2.1 compared to version 2.0?
ANS: Enhancements have been made to reduce or simplify data requirements, provide reviewers with AM/PM and forecast intersection traffic data and better predict alternative cost estimates. However, the minor changes to scoring criteria and alternatives analysis should not substantially impact alternative scoring and ranking compared to the previous software version. Specific changes include:

- Intersection graphics and text have been enhanced, including photos and document links for each juncture type
- Several intersection types were added, including signalized and unsignalized Diamond and Dual Roundabout interchanges
- Users are asked to input both AM and PM peak period volumes and analysis results. The volume input data is used to project existing and design year entering intersection volumes and average daily traffic for approaches. Stage 2 operations analysis use a weighted average of AM and PM intersection delay and V/C results.
- In Stage 2, users can now analyze and compare intersection operations by Delay and V/C or Network Delay
- Right-of-Way impact is selected by land use type and cost per acre is auto-populated from countywide averages
- Additional CMF data is now auto-populated using FHWA CMF Clearinghouse and other resources as appropriate

Question 2: Several intersection control alternatives include multiple intersections. How is intersection delay compared to the base intersection conditions of a singular intersection?

ANS: Engineering judgement is required on a case-by-case basis, but the general principle is to add the delay incurred by vehicles with longer travel paths weighed by the number (or percentage) of those vehicles making that movement.

Question 3: Not all tools give overall intersection delay and V/C ratios. Which delay value should I choose?
ANS: For unsignalized intersections (where one or more movements are not required to stop and thus have zero delay), use the worst-case approach movement delay. If all intersection movements have some form of intersection control (yield, stop or signal), use a weighted average of each approach delay multiplied by the volume on each approach.

Question 4: How do I analyze multiple intersections along a corridor?
ANS: The ICE tool is designed for individual intersection analyses, but an ICE analysis is required for all public street intersections and major driveways along a corridor (unless otherwise stipulated in the ICE waiver section). Use engineering judgement in the recommendation of intersection control choices to ensure corridor continuity (as appropriate) and document intersection control recommendations that are not ranked highest but provide better continuity along the overall corridor.

Question 5: For an ICE Waiver, when is the traffic and crash data required and when is it optional?
ANS: Crash data is required for all existing intersections. ADT's are required if available (from counts if collected or from the nearest GDOT traffic count station site). Capacity data is optional unless needed to justify the basis of the waiver request (i.e. required for RIRO where the ICE process is being waived altogether to show that it will operate acceptably).

Question 6: Which worksheets should be printed and included in an ICE submittal?
ANS: Submissions for and ICE Waiver require submission of the singular Waiver worksheet. Full ICE submissions should include the Introduction, Stage 1 and Stage 2 worksheets, with CostEst (if used) and Scoring worksheets as optional.

For questions or comments about this ICE Tool, contact Daniel Trevorrow (DTrevorrow@dot.ga.gov) or Jonathan Reid (jonathan.reid@arcadis.com)

## Tool Version Tracking

| Version | Released | Tool Updates: |
| :---: | :---: | :--- |
| 2.0 | $7 / 17 / 2017$ | - Initial ICE Tool release date, corresponding with ICE Policy release date of July 1,2017 |
| 2.01 | $9 / 18 / 2017$ | - Modifications made to the Waiver type to include other submittal categories and data requirements |
| 2.1 | $1 / 5 / 2018$ | - Intersection worksheet graphics/text have been enhanced, including photos \& document links for interchange types <br> - Added intersection types, including Diamond Interchanges (signal \& unsignalized) and Dual Roundabout interchange <br> - Cost of Right-of-Way (by acre) for rural and urban parcels are now auto-populated based on individual countywide data <br> - Additional CMF data is now auto-populated using FHWA CMF Clearinghouse and other resources as appropriate <br> - Users can now choose to analvze and comnare intersection onerations bv Delav and V/C or Network Delav |
| 2.11 | $1 / 25 / 2018$ | - Fixed bug to report ROW costs for all Counties |
| 2.12 | $2 / 20 / 2018$ | - Fixed bug to in calculating B/C ratio for Safety Funded Projects <br> - Updated Mult-File Summary sheet to iclude PI\#, waiver and Stage 1 and Stage 2 Descision Matrix w/signature line |
| 2.13 | $3 / 12 / 2018$ | - Refomatted volume inputs for easier data export; Differentiated existing, opening and design years; added new CMFs |
| 2.14 | $8 / 6 / 2018$ | - Minor bug fixes; Updated headers to include new GDOT logo <br> - Updated several CMF's and added single RT and LT lanes <br> - Added graphic of Opening \& Design Year volumes (auto-generated based on growth rates or user input) |

Unsignalized At-Grade Intersections
 through lanes on the bridge (no turn lane storage lanes) and the elimination of signal control at the ramp terminals. There are a total of 16 baseline conflict points (over two intersections).
Also known as: Teardrop Interchange


Offset-Tee Intersection: Creates an offset of minor street approaches to form 2 intersections with the major roadway separated by some distance (between 300 ' and 500 '). Through movements on the minor street "jog" using the major street (right-turns followed by left-turns or vice versa). The Offset-T has a total of 18 baseline conflict points (over two intersections).
Also known as: Paired Intersection
Double Roundabout Interchange: Use of single or dual lane roundabouts at traditional diamond interchange ramp terminals. The use of roundabouts requires only
Conventional Minor Street or All-Way Stop: At minorstreet stop (2-way stop) intersections, vehicles on minor street stop and give right-of-way to major street. At allway stop (AWS) intersections, all vehicles must stop and take turns entering the intersection. Both (4-leg) intersection types have 32 baseline conflict points and have limited operational and safety benefits as traffic volumes become significant.
Mini Roundabouts: Roundabout type characterized by a small diameter and traversable central island; offers most of the benefits of single-lane roundabouts with added benefit of a smaller footprint; best suited to lowerspeed environments and where environmental constraints preclude use of a larger roundabout with a raised central island. Mini-roundabouts are emerging in U.S. in states including MD, MI and GA.

Single-Lane Roundabouts: Form of circular intersection in which traffic travels counterclockwise around a central island and in which entering traffic must yield to circulating traffic. Circulating traffic has priority with entries controlled by yield. Geometry slows all traffic into and thru the roundabout. At a 4-leg roundabout there are 8 baseline conflict points.
Also known as: Modern Roundabout
Multilane Roundabouts: Share same circulatory travel and yield-at-entry in single-lane roundabouts, but include multiple entry and circulatory lanes for one or more approaches that must accommodate vehicles traveling side by side. Important design features include proper entry path alignment and geometry, signing and marking that allows entry to exit paths without forcing a lane change in the circle.
Restricted Crossing U-Turn (RCUT): Redirects minor street left turn movements as right-turns followed by a Uturn movement via a downstream directional crossover in the median (+/- 500 feet from the main intersection). An RCUT intersection has 14 conflict points and can provide substantial safety benefits with minor delay increases to some movements
Also known as: "J-turn" intersection
RIRO w/Downstream U-Turn: Redirects minor street thru \& left turn movements as right-turns followed by a Uturn via directional median crossover ( + /- 500 feet from main intersection). Major street lefts are also made indirectly, passing the crossing street and using the same U-turn crossovers in the median. Minor street intersections are reduced to right-in/right-out movements making this the safest intersection type.


Unsignalized High-T: Unsignalized 3-leg intersection features raised channelization to separate "top" thru movement from turning lanes at intersection, allowing the through movement to operate continuously. A high- $T$ intersection has 9 baseline conflict points, the same as a conventional 3-leg.
Also known as: "Seagull" intersection


Signalized At-Grade Intersections


Median U-Turn: Left turn movements otherwise occurring at the main intersection are made via U-turns in the median, preceding or following right turns. U-turns may be only on major roadway or on both major and minor roadways. A conventional MUT has 16 baseline conflict points and has shown significant operational and safety benefits.
Also known as: Indirect Left, Michigan Left, MUT


Signalized RCUT: Similar to the Median U-turn but features break in cross-street traffic that allows signals on opposite directions to operate independently. Left turns can make directly turns onto the minor road but minor road thru and left turn movements are made using the directional U-turn crossovers. An RCUT has 14 baseline conflict points (over 3 intersections).
Also known as: Superstreet
Displaced Left-Turn (DLT): Left turn traffic crosses opposing lanes in advance of main intersection and are stored in additional lanes. At main intersection, thru and left turns can be made simultaneously during same signal phase. A full DLT (both routes) has 28 baseline conflict points; a partial DLT (one route) has 30 baseline conflict points.
Also known as: Continuous Flow Intersection Continuous Green-T: Three-leg intersection that features raised channelization to allow the "top" through movement to operate under continual green. The opposite direction intersects with the major and minor street lefts at a signalized intersection (minor left turns merge with the continual through movement downstream). A Continuous Green-T has 9 baseline conflict points, the same as a conventional 3 -leg. Jughandle: Much like an at-grade diamond interchange, ramps on the major street diverge from the right side in advance of a cross street intersection, removing the left turn movement from directly at the cross-street intersection. Major street left turns are made at minor, stop-controlled intersections on the cross-street. Left turns from the cross-street remain as direct movements at the main intersection.
Quadrant Roadway: Left turns are removed from the main intersection via an additional roadway in one intersection quadrant. Left-turn movements are routed from the arterial and cross-street (using unique turning paths for each approach) onto the quadrant roadway to complete the left turn movement at the quadrant roadway "minor" T-intersections. A Quadrant Roadway has 28 baseline conflict points (over 3 intersections).
Diverging Diamond Interchange (DDI): All traffic crosses over to left side of road at first ramp terminal intersection before crossing back over at second ramp terminal. Crossover movements allow left turns to be made unopposed. A DDI has a total 14 baseline conflict points (over two intersections) and has shown both operational and safety benefits.
Also known as: Double Crossover Diamond
Single Point Urban Diamond (SPUI): Free-flow major street thru movements are provided by creating a separate, signalized intersection of major street turning movements with the cross-street on a separate grade, creating an intersection either under or over the priority thru roadway. Right turns are made at unsignalized ramps separated from the main intersection.



## 2019 Opening Year Volumes



2018 Design Year Volumes


| Design Year Volumes \＃DIV／0！ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EB SR3 |  |  | （0） | （0） | （0） | （0） |  |  |  |
|  |  |  | 0 | 20 | 0 | 5 |  |  |  |
|  |  |  | Peds $\hat{\downarrow}$ | $\stackrel{y}{4}$ | $\checkmark$ | $\stackrel{ }{4}$ | $\xrightarrow{\text { Peds }}$ | 0 | （0） |
| $\begin{aligned} & \text { 芫 } \\ & \substack{\text { 2 }} \end{aligned}$ | （0） | 80 | 人） | 2018 Intersection Daily Entering Volume： \＃DIV／0！ |  |  | E | 30 | （0） |
|  | （0） | 840 | $\Rightarrow$ |  |  |  | $\stackrel{\square}{\square}$ | 850 | （0） |
|  | （0） | 10 | $\Rightarrow$ |  |  |  | ${ }^{1}$ | 130 | （0） |
|  | （0） | 0 | Peds | 尔 | 介 | ， | $\downarrow^{\text {Peds }}$ | WB SR 3 |  |
|  |  |  | 㐫 | 10 | 10 | 165 | 0 |  |  |
|  |  |  | 믕 | （0） | （0） | （0） | （0） |  |  |
|  |  |  |  |  | \＃DIV／0 |  |  |  |  |

Introduction：In 2005，SAFETEA－LU established the Highway Safety Improvement Program（HSIP）and mandated that each state prepare a Strategic Highway Safety Plan（SHSP）to prioritize safety funding investments．Intersections quickly became a common component of most states＇SHSP emphasis areas and HSIP project lists，including Georgia＇s SHSP．Intersection Control Evaluation（ICE）policies and procedures represent a traceable and transparent procedure to streamline the evaluation of intersection control alternatives，and further leverage safety advancements for intersection improvements beyond just the safety program．Approximately one－third of all traffic fatalities and roughly seventy five percent of all traffic crashes in Georgia occur at or adjacent to intersections．Accordingly，the Georgia SHSP includes an emphasis on enhancing intersection safety to advance the Toward Zero Deaths vision embraced by the Georgia Governor＇s Office of Highway Safety（GOHS）．This ICE tool was developed to support the ICE policy，developed and adopted to help ensure that intersection investments across the entire Georgia highway system are selected，prioritized and implemented with defensible benefits for safety towards those ends．

Tool Goal：The goal of this ICE tool is to provide a simplified and consistent way of importing traffic，safety，cost，environmental impact and stakeholder posture data to assess and quantify intersection control improvement benefits．The tool supports the ICE policy and procedures to provide traceability，transparency，consistency and accountability when identifying and selecting an intersection control solution that both meets project purpose and reflects overall best value in terms of specific performance－based criteria．
Requirements：An ICE is required for any intersection improvement（e．g．new or modified intersection，widening／reconstruction or corridor project，or work accomplished through a driveway or encroachment permit that affects an intersection）where：1）the intersection includes at least one roadway designated as a State Route（State Highway System）or as part of the National Highway System；or 2）the intersection will be designed or constructed using State or Federal funding．In certain circumstances where an ICE would otherwise be required，the requirement may be waived based on appropriate evidence presented with a written request．（See the＂Waiver＂tab to review criteria that may make a project waiver eligible and for instructions to submit a waiver request to the Department）．An ICE is not required when the proposed work does not include any changes to the intersection design，involves only routine traffic signal timing and equipment maintenance，or for driveway permits where the driveway is not a new leg to an already existing intersection on either 1）a divided，multi－lane highway with a closed median and only right－in／right－out access or 2 ）an undivided roadway where the development is not required to construct left and／or right turn lanes（as per the Driveway Manual and District Traffic Engineer）．
Two－Stage A complete ICE process consists of two（2）distinct stages，and it is expected that the respective level of effort for completing both stages of ICE will correspond to the Process：magnitude and complexity of the intersection．Prior to starting an ICE，the District Traffic Engineer and／or State Traffic Engineer should be consulted for advice on an appropriate level of effort．The Stage 1 and Stage 2 ICE forms are designed minimize required data inputs using drop－down menu choices and limiting text entry．All fields shaded grey include drop down menu choices and all fields shaded blue require data entry．All other cells in the worksheet are locked．
Stage 1：Stage 1 should be conducted early in the project development process and is intended to inform which alternatives are worthy of further evaluation in Stage 2．Stage 1 serves Screening as a screening effort meant to eliminate non－competitive options and identify which alternatives merit further considerations based on their practical feasibility．Users should Decision use good engineering judgement in responding to the seven policy questions by selecting＂Yes＂or＂No＂in the drop－down boxes．Alternatives should not be summarily Record eliminated without due consideration，and reasons for eliminating or advancing an alternative should be documented in the＂Screening Decision Justification＂column．
Stage 2：Stage 2 involves a more detailed and familiar evaluation of the alternatives identified in Stage 1 in order to support the selection of a preferred alternative that may be advanced
Alternative to detailed design．Stage 2 data entry may require the use of external analysis tools to determine costs，operations and／or safety data that，combined with environmental and Selection stakeholder posture data，form the basis of the ICE evaluation．A separate＂CostEst＂worksheet tab helps users develop pre－planning－level cost estimates for each Stage 2 Decision alternative evaluated，and a separate Users Guide has been prepared to give guidance on Stage 1 and Stage 2 data entry．Once all data is entered，each alternative is scored Record and ranked，with the results reported at the bottom of the Stage 2 worksheet to inform on the best of the intersection controls evaluated for project recommendation．
Documentation：A complete ICE document consists of the combination of the outputs from either a completed and signed waiver form or both Stage 1 and Stage 2 worksheets（along with supporting costing and／or environmental documentation），to be included in the approved project Concept Report（or equivalent）or as a stand－alone document．

| GDOT PI\# | N/A |
| :--- | :---: |
| Project Location: | SR 3 @ Old Dixie hwy |
| Prepared by: | D6 TrafficOperations |
| Analyst: | Manara ALI |
| Date: | 12/30/2019 |
| Answer "Yes" or "No" to each policy question for <br> each control type to identify which alternatives <br> should be evaluated in the Stage 2 Decision <br> Record; enter justification in the rightmost column |  |
| Intersection Alternative (see "Intersections" tab for <br> detailed description of intersection/interchange type) |  |

Note: Up to 5 alternatives may be selected and evaluated; Use this ICE Stage 1 to screen 5 or fewer alternatives to evaluate in Stage 2

Screening Decision

| Conventional (Minor Stop) | No | No | No | No | Yes | No | Yes | Current Intersection set up |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Conventional (All-Way Stop) | No | No | No | No | Yes | No | No | Results do not warrantan All-Way Stop |
| Mini Roundabout | No | Yes | Yes | No | Yes | No | No | N/A |
| Single Lane Roundabout | No | Yes | Yes | No | Yes | No | No | N/A |
| Multilane Roundabout | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Considered for further Analysis |
| RCUT (stop control) | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Considered for further Analysis |

$\square=$ Intersection type selected for more detailed analysis in Stage 2 Alternative Selection Decision Record

GDOT PI \# (or N/A) N/A County: Whitfield Project Location: SR 3 @ Old Dixie hwy Existing Intersection Control: Conventional (Minor Stop)

GDOT District: 6 - Cartersville
Area Type: Urban

ICE Version 2.14 | Revised 08/03/2018 Date: 12/30/2019
Agency/Firm: D6 TrafficOperations Analyst: Manara ALI
Type of Analysis: Conventional Non-Safety Funded Project

## Opening / Design Year Traffic Operations

| Intersection meets signal/AWS warrants? | Meets Signal Warrants |  |
| :--- | :---: | :---: |
| Traffic Analysis Measure of Effectiveness | Intersection Delay |  |
| Traffic Analysis Software Used | HCS 2010 |  |
| Analysis Time Period | AM Peak Hr | PM Peak Hr |
| 2019 Opening Yr No-Build Peak Hr Intersection Delay | 108.1 sec | 0.0 sec |
| 2019 Opening Yr No-Build Peak Hr Intersection V/C | 0.51 | 0.00 |
| 2018 Design Yr No-Build Peak Hr Intersection Delay | 0.0 sec | 0.0 sec |
| 2018 Design Yr No-Build Peak Hr Intersection V/C | 0.00 | 0.00 |
|  |  |  |

Complete Streets Warrants Met?
$\square$ PEDESTRIANS
$\square$ BICYCLES
$\square$ TRANSIT

| Crash Data:Enter 5 most recent <br> years of intersection crash data | Crash Severity |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | PDO | Injury Crash* | Fatal Crash* |

* Number of crashes resulting in injuries / fatalities, not number of persons


[^1]Provide additional comments and/or explain any unique analysis inputs, or results (as necessary):

Project Information
Location: SR 3 @ Old Dixie hwy GDOT PI \# (or N/A): N/A
Existing Intersection Control: Conventional (Minor Stop) Type of Analysis: Conventional Non-Safety Funded Project

County: Whitfield
Area Type: Urban
GDOT District: 6 - Cartersville

ICE Version 2.14 | Revised 08/03/2018
Date: 12/30/2019
Agency/Firm: Analyst: Manara ALI Major Street Direction: East/West

| Table 1: Existing Conditions | EB SR 3 |  |  | WB SR 3 |  |  | NB Old Dixie hwy |  |  | SB Old Dixie hwy |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | Left Turn | Thru | Right Turn | Left Turn | Thru | Right Turn | Left Turn | Thru | Right Turn | Left Turn | Thru | Right Turn |
| Number of Lanes | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Widths* | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0{ }^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0 '$ | $0^{\prime}$ | $0^{\prime}$ |
| Bay Length** | 0' |  | 0' | $0^{\prime}$ |  | $0^{\prime}$ | $0^{\prime}$ |  | $0^{\prime}$ | $0^{\prime}$ |  | 0' |
| Median Width |  | $0^{\prime}$ |  |  | $0^{\prime}$ |  |  | $0^{\prime}$ |  |  | $0^{\prime}$ |  |
| Right-of-Way | $0^{\prime}$ |  |  |  |  | $0^{\prime}$ |  |  |  |  |  |  |
| Table 2: Proposed Conditions | Conventional (Minor Stop) | Multilane <br> Roundabout | RCUT (stop control) | Offset Left Turn <br> Lanes Traffic Signal |  | Site Context |  |  |  | Intersections |  |  |
| Proposed Pavement Type | None | None | None | None | None | Topography: Traffic Mgmt Plan: Project Size: |  | Rolling |  | Signal Poles |  | Mast Arm |
| Reimbursable Utility: | Moderate | Moderate | Moderate | Moderate | Moderate |  |  | Maintain Traffic |  | Design Vehicle <br> Existing Interchange? |  | WB-67 |
| \# of Driveway(s) Impacted | 0 | 0 | 0 | 0 | 0 |  |  | Single Intersection |  |  |  | No |
| Modify/Replace Traffic Signal | 0 | 0 | 0 | 0 | 0 | Cost Multipliers |  |  |  |  |  |  |
| Lighting Poles (ea) | 0 | 0 | 0 | 0 | 0 |  |  |  | Inscribed DIA - Mini |  |  | 80 |
| Flashing Beacons (ea) | 0 | 0 | 0 | 0 | 0 |  |  |  | Inscribed DIA - Single |  |  | 140 |
| RFB/PHB Ped Crossings (ea) | 0 | 0 | 0 | 0 | 0 | Grading Complete: <br> Reimbursable Utility: |  | 20\% | Inscribed DIA - Multi Circulating Lane Width |  |  | 200 |
| New/Replace Sidewalks (LF) | $0 '$ | $0 '$ | $0 '$ | $0 '$ | $0 '$ |  |  | 5\% |  |  |  | 18 |
| New/Replace Cross Drains (LF) | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | Traffic Control: Project Size: |  | 20\% | ROW Costs |  |  |  |
| New/Replace Guardrail (LF) | $0^{\prime}$ | $0 '$ | $0 '$ | $0{ }^{\prime}$ | $0^{\prime}$ |  |  | 0\% | Prevalent ROW Type: |  | Mixed (Average) |  |
| New Retaining Wall (LF) | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | $0^{\prime}$ | Prelim Engineering: <br> Project Contingency: |  | 15\% | ROW Cost/Acre: ROW Multiplier: |  | \$69,563 |  |
| Bridge:New/Widen/Replace (sqft) | 0 | 0 | 0 | 0 | 0 |  |  | 20\% |  |  | 1.6 |  |
|  | \$0 | \$0 | \$0 | \$0 | \$0 |  |  |  |  |  |  |  |

## Table 3: Control Type Cost Breakdown

|  | Per Ln Mi |  | Convention | inor Stop) | Multilane | undabout | RCUT ( | control) | Offset Le | Lanes | Traffic | ignal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pay Item | Unit Cost | Unit Cost | Quantity | Cost | Quantity | Cost | Quantity | Cost | Quantity | Cost | Quantity | Cost |
| New Construction (Base \& Pave) | \$500K/LM | \$9.47/sqft | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Roadway Mill and Overlay | \$64K/LM | \$1.21/sqft | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Urban C\&G/Drainage - both sides | 441-6720 | \$19.08/LF | 0 | \$0 | 2,400 | \$60,903 | 3,600 | \$68,688 | 0 | \$0 | 4,000 | \$76,320 |
| Rural Typ Drainage - both sides | \$150K/LM | \$2.84/LF | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Concrete Island (sqyd) | n/a | \$51.58/syd | 0 | \$0 | 0 | \$0 | 500 | \$25,790 | 0 | \$0 | 0 | \$0 |
| Median Landscaping | \$100K/LM | \$1.89/LF | 0 | \$0 | 3,600 | \$9,068 | 5,400 | \$10,227 | 0 | \$0 | 0 | \$0 |
| Typical Driveways Impacted (ea) | n/a | \$7,500 ea | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Typical E\&S Control Temp/Perm | \$150K/LM | \$34.09/LF | 0 | \$0 | 1,200 | \$54,409 | 1,800 | \$61,364 | 0 | \$0 | 2,000 | \$68,182 |
| Roundabout Truck Apron (sqft) | n/a | \$10.25/sfft | 0 | \$0 | 3,707 | \$50,540 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Signing \& Marking | \$0 | \$22.73/LF | 0 | \$0 | 1,200 | \$36,277 | 1,800 | \$40,914 | 0 | \$0 | 2,000 | \$45,460 |
| Flashing Beacon (ea) | n/a | \$20,000 ea | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| New Traffic Signal (Mast Arms) | 674-1000 | \$182,575ea | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Lighting (per pole) | n/a | \$5,607 ea | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Signalized Ped Crossings (ea) | n/a | \$19,637 ea | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| 6' Sidewalk (LF) | n/a | \$49.23/LF | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| New/replace cross drains (LF) | n/a | \$41.31/LF | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Typical Guardrail (LF) | n/a | \$65.56/LF | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Retaining Wall (LF) | n/a | \$808.52/LF | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Bridge widen/replace (SF) | n/a | \$210/sqft | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Env Costs (from Stage 2 impacts) | n/a | n/a | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 | 0 | \$0 |
| Grading Complete - 20\% | n/a | n/a |  | \$0 |  | \$84,268 |  | \$41,397 |  | \$0 |  | \$0 |
| Traffic Control-20\% | n/a | n/a |  | \$0 |  | \$56,179 |  | \$41,397 |  | \$0 |  | \$0 |
| Reimbrusable Utility | n/a | n/a |  | \$0 |  | \$10,560 |  | \$10,349 |  | \$0 |  | \$9,498 |
| Preliminary Engineering - 15\% | n/a | n/a |  | \$0 |  | \$42,134 |  | \$31,047 |  | \$0 |  | \$28,494 |
| Contigency - 20\% | n/a | n/a |  | \$0 |  | \$56,179 |  | \$41,397 |  | \$0 |  | \$37,992 |
| ROW Cost/Acre: Mixed (Average) | n/a | \$69,563ac |  | \$0 |  | \$77,292 |  | \$103,481 |  | \$0 |  | \$0 |
| Add'I ROW / Displacement / Demo | n/a | n/a |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| ROW Multiplier - 1.6 | n/a | n/a |  | \$0 |  | \$46,375 |  | \$62,089 |  | \$0 |  | \$0 |
| Project Scale Reduction - 0.0\% | n/a | n/a |  | \$0 |  | \$0 |  | \$0 |  | \$0 |  | \$0 |
| Grand Total Costs |  |  |  | \$0 |  | \$584,000 |  | \$538,000 |  | \$0 |  | \$266,000 |

Table 4: Assumption Adjustments/Quantity Overrides

| Alternative Evaluated | Assumptions: | Pavement | Calculated <br> ROW (ac) | User <br> Override* | Calculated <br> Pavement | User <br> Override | Major ST <br> Const Limits | User <br> Override* $^{*}$ | Minor ST <br> Const Limits | User <br> Override* |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conventional (Minor Stop) | N/A | None | 0.00 | 0.0 | 0 | 0.0 | 50 | 0.0 | 50 | 0.0 |
| Multilane Roundabout | --select one-- | None | 1.11 | 0.0 | 18,549 | 0.0 | 600 | 0.0 | 600 | 0.0 |
| RCUT (stop control) | --select one-- | None | 1.49 | 0.0 | 29,358 | 0.0 | 1,300 | 0.0 | 500 | 0.0 |
| Offset Left Turn Lanes | N/A | None | 0.00 | 0.0 | 0 | 0.0 | 0 | 0.0 | 0 | 0.0 |
| Traffic Signal | --select one-- | None | 0.0 | 0.0 | 16,000 | 0.0 | 1,000 | 0.0 | 1,000 | 0.0 |

## Waiver Request - Level 1

In certain circumstances where an ICE would otherwise be required, an ICE may be waived based on appropriate evidence presented with a written request. Scenarios in which an ICE waiver request may be considered include:

1. Proposed improvements do not substantially alter the character of the intersection, and are considered minor in nature, such as extending existing turn lane(s) or modifying signal phasing at an existing traffic signal
2. The intersection consists of a public roadway intersecting a divided, multilane roadway where the access will be limited to a closed median with only right-in/right-out access that will operate acceptably; or

3 The intersection is along an undivided, two-lane roadway that will not be widened and meets the following criteria:

- Low risk in terms of exposure (total intersection entering volume less than 1,000 vehicles /day)
- Latest 5 years of crash history is not indicative of a crash problem (no discernible crash patterns coupled with low crash frequency and severity)
- Layout has no unusual or undesirable geometric features (such as restricted sight distance)
- The proposed changes are not expected to adversely affect safety

If only one alternative is determined to be feasible from the ICE Stage 1, then a waiver may be submitted in lieu of completing ICE Stage 2. The waiver must clearly explain why there is no other feasible alternative. A Waiver Form should also be submitted to document an agreed upon decision to select a preferred alternative other than the highest scoring alternative in Stage 2.

ICE waiver forms with supporting documentation should be submitted for approval to the Office of Traffic Operations or District Engineer (depending on Waiver level). Questions regarding the waiver process should be routed to the State Traffic Engineer.

Project Information: $\begin{gathered}\text { Location: SR } 3 @ \text { Old Dixie hwy } \\ \text { County: Whitfield }\end{gathered}$
GDOT District: $6-$ Cartersville
Area Type: Urban
Existing Intersection Control: Conventional (Minor Stop)
Traffic and Operations Data: ${ }^{1}$

| Intersection meets signal/AWS warrants? Traffic Analysis Type: | Meets Signal Warrants |  |
| :---: | :---: | :---: |
|  | Intersection Delay |  |
| Existing Avg Daily Traffic (Major Street): | 0 |  |
| Existing Avg Daily Traffic (Minor Street): | 0 |  |
| Analysis Period: | AM Peak | PM Peak |
| 2019 Opening Yr Peak Hour Intersection Delay: | 108.1 sec | 0.0 sec |
| 2019 Opening Yr Peak Hour Intersection V/C: | 0.51 | 0.00 |
| 2018 Design Yr Peak Hour Intersection Delay: | 0.0 sec | 0.0 sec |
| 2018 Design Yr Peak Hour Intersection V/C: | 0.00 | 0.00 |

${ }^{1}$ Crash data required for all existing intersections. ADT's required if available (from data collected or neares GDOT count station site). Capacity data is optional unless needed to justify basis of the waiver request.

GDOT PI \# (or N/A): N/A
Requested By: D6
Prepared By: D6 TrafficOperations
Analyst: Manara ALI
Date: 12/30/2019
Waiver Request Type: GDOT PDP Project


* Number of crashes resulting in injuries / fatalities, not number of persons

| Description of Work / <br> Justification for Waiver <br> (Required): |  |
| ---: | ---: |
| At this stage it is recommended that the Two-way Stop Control be replaced with a Multi-lane Roundabout |  |
| Proposed Intersection Control: |  |

REQUESTED BY:

Title: $\qquad$

APPROVED BY: $\qquad$ Date:

Name:

## Project Information

GDOT District: 6-Cartersville
Requested By: D6
County: Whitfield
Project Location: SR 3 @ Old Dixie hwy
Existing Intersection Control: Conventional (Minor Stop)

## Environmental Factors

In the box below, document any significant environmental factors for any alternative considered. Include a plan and costs for mitigation that retains the proposed intersection type as a viable alternative. Include in ICE documentation package only if one or more alternatives have significant impacts.

Proposed Intersection Control \#1: Conventional (Minor Stop)
None

Proposed Intersection Control \#2: Multilane Roundabout
None

Proposed Intersection Control \#3: RCUT (stop control)
None

Proposed Intersection Control \#4: Offset Left Turn Lanes
None

Proposed Intersection Control \#5: Traffic Signal
None

Welcome to GDOT's Roundabout Analysis Tool. This tool is designed for the user to determine the functionality of a proposed roundabout. The analysis is based on the Highway Capacity Manual 2010 Edition and 6th Edition Methodologies, NCHRP Report 672, and FHWA's Roundabout Informational Guide. Please read the notes in the Instructions tab before using the spreadsheet.

| Analyst: | Manara ALI |
| :---: | :---: |
| Agency/Company: | GDOT |
| Date: | 12/23/2019 |
| Project Name or PI\#: |  |
| Year, Peak Period: | Peak Hour |
| County/District: | Whitfield/District 6 |
| Intersection: | SR 3 @ Old Dixie Hwy/ Five Springs Rd |

## Insert Project Information Here in the BLUE SPACE. This information is linked to the Mini, Single Lane and Multi Lane Worksheets.

## Roundabout Considerations Worksheet

Roundabouts may not operate well if there is too much traffic entering the intersection or if the percentage of traffic on the major road is too high. Candidate intersections shall be analyzed to determine whether a roundabout will perform acceptably. Shown below are planning level thresholds. A capacity analysis should be performed to determine lane configuration based on traffic volumes.

| \# of circulatory lanes | ADTs (current/ build year) | Condition met? | \% traffic on Major Road | Condition met? |
| :---: | :---: | :---: | :---: | :---: |
| Mini | less than 15,000 | Yes | less than 90\% | Yes |
| Single Lane | less than 25,000 | Yes | less than 90\% | Yes |
| Multi-Lane | less than 45,000 | Yes | less than 90\% | Yes |

Other things to consider when evaluating roundabouts as an alternative are Right of Way, sight distance, environmental impacts, and access to adjacent properties.

## Volume Information (for Analysis Time Period)

1 Enter the Major/Minor Street ADT Volumes in the Chart below:

|  | Volumes | Split |  |
| ---: | ---: | ---: | :---: |
| Major Street | 10,600 | $84 \%$ |  |
| Minor Street | 2,010 | $16 \%$ |  |
| Total volumes | 12,610 |  |  |

## Proximity to Other Intersections

2 How close is the nearest signal (miles or feet)? $\quad 0 \mathrm{mi} \quad 1800^{\prime}$

3 Is the proposed intersection located within a coordinated signal network? $\qquad$ Go up to next sectien...- - - -

Georgia Department of Transportation

## $r>$ Proposed Design Configuration Chart

## Directions for this Section only: (see Instructions Tab for other sections)

1. Select the type of roundabout you are analyzing.
2. Key in the number of approaches and the street names at the proposed intersections.
3. Complete the Approach Characteristics Chart:
a. Select the Street Name from the pulldown menu for each approach leg
b. Select the Lane Type for each entry apporach lane
*The first box is the inner lane, the second box is the outer lane
c. Select Yes or No if a right turn bypass will be added to each approach leg

## Roundabout Characteristics

| \| Roundabout Type: | Single Lane |
| :---: | :---: |
| \\| \# of Approaches: | 2 |
| \| Name of Streets: | SR 3 |
| I | Old Dixie Hwy |
|  | Five Springs Rd |
| 1 |  |
| I |  |


| Mini/Single Lane | Chart Key: |  |
| :---: | :---: | :---: |
|  | Street Name |  |
| Multi-lane | All |  |
|  | Bypass? |  |
|  | Stree | Name |
|  | Inner Ln | Outer Ln |
|  | Bypass? |  |

Approach Leg Characteristics:

| North Leg (1) |  | NE Leg (2) | East Leg | SE Leg (4) |
| :---: | :---: | :---: | :---: | :---: |
| Street Name: <br> Entry Lane Config <br> Bypass to Adj Leg? | Five Springs Rd |  | SR 3 |  |
|  | All |  | All |  |
|  | $\begin{array}{\|l\|} \hline \text { No } \\ \hline \text { South Leg (5) } \\ \hline \end{array}$ |  | No |  |
|  |  | SW Leg (6) | West Leg | NW Leg (8) |
| Street Name: | Old Dixie Hwy |  |  |  |
| Entry Lane Config | All |  | All |  |
| Bypass to Adj Leg? | No |  | No |  |



## Worksheet Instructions

This workbook contains an analysis spreadsheet for a mini, single lane and a multi lane roundabout. It also has an option to analyze a bypass lane if it is included as a design option. The worksheets are protected to prevent accidental changing of formulas except in the General/Site Information, Volumes, and Volume Characteristics sections.
Insert values into Blue Boxes to avoid accidental changes in the spreadsheet.

## Common Items to all calculators

## General \& Site Information

Analyst name, work organization, today's date, project name/PI\#, intersecting street names, time period (i.e. 4:00-5:00 PM), analysis year (existing, 2030 Build, etc), and county/district should be entered.

The roundabout calculator can support up to eight legs for maximum geometric flexibility (leg placement). Highlighting the legs used on a printed version of the provided diagram can help when routing volumes.

## Volumes

Volumes are entered in columns that correspond to the existing or proposed roundabout legs. Volumes are entered as origin destination pairs with the column heading denoting the origin and row heading denoting the destination. For example, volumes arriving on the north leg and making a left turn onto the east leg are coded in the cell intersection of the N column and the E row. This format makes it possible if leg placement is not standard or is more than four legs where there might be more than one discrete left or right turn. This format also allows for u-turns to be coded into the model. However the engineer shoud take care when entering the OD pairs not to accidentally code a left turn, through movement, or right turn as a u-turn. Entering a u-turn value will cause the background of that value to change to yellow. This helps the user recognize when a u-turn value has been entered.

## Volume Characteristics

Changing the peak hour factor (PHF) and the percentage of trucks, SU/buses, or bicycles will cause the background of these values to change to yellow and dark blue respectively. This will allow the user and reviewer to keep track of changes to the default values.

A PHF derived from current counts should be used to replace the default PHF. The truck equivalency factor is normally set at 2.0. However, this value can change based on facility type (i.e. two-lane highway versus multilane highway) or if the approach is on a grade. Current counts should be used to determine the percent of trucks and bicycles on an approach. To change the equivalency factors, update the Pink Boxes in the Equivalency Factor table.

The heavy vehicle factor will be automatically computed and will be combined with the PHF to determine flow rates.

## Entry/Conflicting Flows

This section automatically computes the entry flows for each leg and the corresponding conflicting flow. No input is needed.

## Results

Results will only be shown for columns where entry volumes have been entered. This section computes the entry capacity based on the HCM formula and reports the conflicting flow, the entry leg volume-to-capacity ratio, the approach control delay, the approach LOS, and the 95th percentile queue. The 95th percentile queue is based the HCM formula for calculating 95th Queue length at unsignalized intersections. The HCM 2010 and 6th Edition capacity models are based on an analytical method based on gap acceptance behavior on roundabouts in the United States.

## Mini Roundabout Calculator Notes

## Roundabout Type

This worksheet calculates values for mini roundabouts. Mini roundabouts have fully mountable central islands and smaller diameters, generally below 100 ft . There may be right turn bypasses on the approaches but only one circulating lane in the circulatory roadway

## Single Lane Calculator Notes

## Roundabout Type

This worksheet calculates values for single lane roundabouts. There may be right turn bypasses on the approaches but only one circulating lane in the circulatory roadway. If you have a hybrid roundabout (1 lane circulatory roadway in some areas and 2 lane circulatory roadway in other areas) it is recommended to use the multilane tab as this tab will allow inputs for any entry/circulating combinations for 1 lane 2 lane hybrid roundabouts.

## Multi-Lane Calculator Notes

## Volumes

This section supports up to two entry lanes with any logical movement configuration that can now be entered in the box that says "SELECT." Use Lane 1 (i.e. N1) for the inside approach lane and Lane 2 (i.e. N2) for the outside approach (curb) lane. If a leg only has a single lane, choose either lane but be consistent.

## Critical Lane Volumes

This section computes the critical lane volumes from the above section by finding the highest volume in each approach lane pair. The critical volume is only used to determine the critical entry flow used in the approach leg $\mathrm{v} / \mathrm{c}$ and control delay equations. In this method, the approach flows are assumed to be in conflict with both circulating lanes. This method using critical lane volumes is NCHRP 572 specific. The HCM Method does not use a critical lane methodology to calculate conflicting flows, but uses the total exiting traffic.

## Results

In addition to the other results as previously discussed, the critical lane entry flow is shown.

## Geometric Variations

## Bypass Lanes

If a bypass lane is included in the roundabout configuration, use the following method:
Any bypass lane volume will need to be subtracted out of the appropriate right turn volume. Insert this subtracted volume into the appropriate space on the bypass analysis chart. This value becomes the bypass entry flow and the conflicting flow is generated from the exit volumes from the roundabout on the exit leg. The capacity generated is based on the bypass lane flow yielding to the exiting flow from the roundabout. The multi-lane bypass lane uses three methods for determining the conflicting flow: default method which generates a conservative value based on the total exiting flow, the HCM Methodology, and a manual method which prompts the user to calculate the projected conflicting volume in the outer most exit lane.

## References:

TRB (2016). Highway Capacity Manual: 6th Edition. A Guide for Multimodal Mobility Analysis. Transportation Research Board, National Research Council, Washington, D.C., U.S.A. ("HCM6")

TRB (2010). HCM 2010: Highway Capacity Manual. Transportation Research Board, National Research Council, Washington, D.C., U.S.A. ("HCM2010").

TRB (2000). Highway Capacity Manual. Transportation Research Board, National Research Council, Washington, D.C., U.S.A. ("HCM2000").

Robinson, B.W., et al., Roundabouts: An Informational Guide, Publication No. FHWA-RD-00-067, Federal Highway Administration, Washington, DC, June 2000.

Rodegerdts, L., Bansen, J., Tiesler, C., Knudsen, J., Myers, E., Johnson, M., Moule, M., Persaud, B., Lyon, C., Hallmark, S., Isebrands, H., Crown, R.B., Guichet, B., O'Brien, A., NCHRP Report 672, Roundabouts: An Informational Guide, Second Edition. Washington, D.C., Transportation Reserach Board, (2010)

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Rodegerdts, L. A. "Reassessment of Roundabout Capacity Models for the Highway Capacity Manual." 4th International Conference on Roundabouts, Seattle, (2014). [http://teachamerica.com/RAB14/RAB1406CRodegerdts/index.htm](http://teachamerica.com/RAB14/RAB1406CRodegerdts/index.htm)
**This workbook was adapted from ODOT's Roundabout Calculator.


#### Abstract

Disclaimer: This Excel workbook is provided for use by persons outside of the Georgia Department of Transportation (GDOT) as information only. GDOT, the State of Georgia, nor its officers or employees, by making this workbook available for use by persons outside of GDOT, do not undertake any duties or responsibilities of any such person or entity who chooses to use this document. This workbook should not be substituted for the exercise of a person's own professional judgment nor the determination by contractors of the appropriate manner and method of construction on projects under their control. It is the user's obligation to make sure that he/she uses the appropriate practices. You are advised to test the program thoroughly before you rely on it. Should the program prove defective, you (and not GDOT or the State of Georgia) assumes the entire responsibility. Any person using this workbook agrees that GDOT will not be liable for any commercial loss; inconvenience; loss of use, time, data, goodwill, revenues, profits, or savings; or any other special, incidental, indirect, or consequential damages in any way related to or arising from use of this workbook.


## Updates:

Version 1.0 (3/17/2009)
Version 1.1 (9/1/2009)

- Improved "START HERE" Page to include Design Worksheet to include Proposed Configuration.
- Condensed Bypass Tabs into the Main Analysis Tabs
- Streamlined "Results" to show level of service for unsignalized only.
- Revised Entry Flow for the UK Model, in the Multi-Lane Tab.

Version 1.2 (8/10/2010)

- Revised Roundabout Type Section to indicate "Standard Single Lane" and "Urban Compact"
- Revised Multi-Lane Tab to include user input for number of conflicting lanes in circulatory roadway for a given approach.

Version 1.3 (9/8/2010)

- Critical Update/Revision to Single Lane Bypass Formula and Multi-Lane Analysis MOEs


## Version 2.0 (9/8/2010)

- Critical Update/Revision to Single Lane and Multi-Lane sheets to conform to HCM 2010 Methodology from the NCHRP 572


## Version 2.1 (2/19/2012)

- Critical Update replaces the UK Model with the Calibrated HCM Model based on Oregon and California site-specific empirical data for critical headway and follow-up headway.

Version 3.0 (3/23/2016)

- Critical Update replaces the single lane models with the HCM 6th Edition Model.
- The multilane models on the Multilane Tab are replaced with the HCM 6th Edition Model.
- PHF is changes to .95 for urban and .92 for suburban
- Various updates to the Instructions Tab


## Version 3.1 (7/25/2016)

- Update corrects the Single Lane Tab to calculate the approach with bypass delay and LOS according to the HCM 6th Edition formulas.

Version 4.0 (2/13/2017)

- Critical Update creates Mini Roundabout Tab, using HCM 2010 Edition for capacity calcuations
- Updated START HERE and INSTRUCTIONS tab to include Mini Roundabouts

Version 4.1 (5/19/2017)

- 'Conditions met?' column with Yes/No options added to START HERE tab beside planning level thresholds
- GDOT logo added to every tab


## General \& Site Information

| Analyst: | Manara ALI |  |
| :--- | :--- | :---: |
| Agency/Co: | GDOT |  |
| Date: | $12 / 23 / 2019$ |  |
| Project or PI\#: |  |  |
| Year, Peak Hour: |  |  |
| County/District: | Peak Hour |  |
| Intersection | Whitfield/District 6 |  |
| Name: |  | SR 3 O Old Dixie Hwy/ Five Springs Rd |
|  |  |  |



| Volumes | Entry Legs (FROM) |  |  |  |  |  | W (7) | NW (8) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N(1) | NE (2) | E (3) | SE (4) | S (5) | SW (6) |  |  |
|  |  |  | 20 |  | 107 |  | 91 |  |
|  |  |  |  |  |  |  |  |  |
|  | 4 |  |  |  | 125 |  | 220 |  |
|  |  |  |  |  |  |  |  |  |
|  | 48 |  | 57 |  |  |  | 5 |  |
|  |  |  |  |  |  |  |  |  |
|  | 37 |  | 289 |  | 1 |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  | 89 | 0 | 366 | 0 | 233 | 0 | 316 | 0 |
| Volume Characteristics | N | NE | E | SE | S | SW | W | NW |
| \% Cars | 100.0\% | 100.0\% | 100.0\% | 100.0\% | 100.0\% | 100.0\% | 100.0\% | 100.0\% |
| \% Heavy Vehicles | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |
| \% Bicycle | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |
| \# of Pedestrians (ped/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| FhV | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| $\mathrm{F}_{\text {ped }}$ | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
|  |  |  |  |  |  |  |  |  |
| Entry/Conflicting Flows | N | NE | E | SE | S | SW | W | NW |
| Flow to Leg \# N (1), pcu/h | 0 | 0 | 22 | 0 | 116 | 0 | 99 | 0 |
| NE (2), pcu/h E (3), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 4 | 0 | 0 | 0 | 136 | 0 | 239 | 0 |
| SE (4), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\mathrm{S}(5), \mathrm{pcu} / \mathrm{h}$ | 52 | 0 | 62 | 0 | 0 | 0 | 5 | 0 |
| SW (6), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| W (7), pcu/h | 40 | 0 | 314 | 0 | 1 | 0 | 0 | 0 |
| NW (8), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry flow, pcu/h Conflicting flow, pcu/h | 97 | 0 | 398 | 0 | 253 | 0 | 343 | 0 |
|  | 377 | 0 | 216 | 0 | 342 | 0 | 118 | 0 |


| HCM 2010 Edition | N | NE | E | SE | S | SW | W | NW |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Entry Capacity, vph | 775 | NA | 910 | NA | 802 | NA | 1004 | NA |
| Entry Flow Rates, vph | 97 | NA | 398 | NA | 253 | NA | 343 | NA |
| V/C ratio | 0.12 |  | 0.44 |  | 0.32 |  | 0.34 |  |
| Control Delay, sec/pcu | 6 |  | 9 |  | 8 |  | 7 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \% Queue (ft) | 11 |  | 56 |  | 34 |  | 38 |  |
| Notes: |  |  |  |  |  |  |  | v 4.0 |
|  |  |  |  |  |  | Unit Legen <br> $\mathrm{vph}=$ vehi <br> PHF = pea <br> $\mathrm{F}_{\mathrm{Hv}}=$ heav <br> pcu = pass | les per h hour fac <br> vehicle <br> nger car | ctor <br> nit |
| Bypass Lane Merge Point Analysis (if applicable) |  |  |  |  |  |  |  |  |
| Bypass Characteristics |  |  | Bypass \#1 | $\begin{gathered} \hline \hline \text { Bypass } \\ \# 2 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \hline \text { Bypass } \\ \# 3 \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Bypass } \\ & \# 4 \end{aligned}$ \#4 | Bypass $\# 5$ <br> \#5 | Bypass $\# 6$ |
| Select Entry Leg from Bypass (FROM) Select Exit Leg for Bypass (TO) <br> Does the bypass have a dedicated receiving lane? |  |  |  |  |  |  |  |  |
| Volumes |  |  |  |  |  |  |  |  |
| Right Turn Volume removed from Entry Leg |  |  |  |  |  |  |  |  |
| Volume Characteristics (for entry leg) |  |  |  |  |  |  |  |  |
| PHF |  |  |  |  |  |  |  |  |
| Fhv |  |  |  |  |  |  |  |  |
| $\mathrm{F}_{\text {ped }}$ |  |  |  |  |  |  |  |  |
| NOTE: Volume Characteristics for Exit Leg are already taken into account |  |  |  |  |  |  |  |  |
| Entry/Conflicting Flows |  |  |  |  |  |  |  |  |
| Entry Flow, pcu/hr Conflicting Flow, pcu/hr |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Bypass Lane Results (HCM 2010 Edition) |  |  |  |  |  |  |  |  |
| Entry Capacity of Bypass, vph Flow Rates of Exiting Traffic, vph V/C ratio Control Delay, s/veh LOS <br> 95th \% Queue (ft) |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Approach w/Bypass Delay, s/veh <br> Approach w/Bypass LOS |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

## General \& Site Information

| Analyst: | Manara ALI |  |
| :--- | :--- | :---: |
| Agency/Co: | GDOT |  |
| Date: | 12/23/2019 |  |
| Project or PI\#: |  |  |
| Year, Peak Hour: |  |  |
| County/District: | Peak Hour |  |
| Intersection | Whitfield/District 6 |  |
| Name: | SR 3 @ Old Dixie Hwy/ Five Springs Rd |  |
|  |  |  |



| Volumes | Entry Legs (FROM) |  |  |  |  |  | W (7) | NW (8) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N (1) | NE (2) | E (3) | SE (4) | S (5) | SW (6) |  |  |
| $\begin{array}{cr} & \mathrm{N}(1), \mathrm{vph} \\ \text { Exit } & \text { NE (2), vph } \\ \text { Legs } & \mathrm{E}(3), \mathrm{vph} \\ \text { (TO) } & \text { SE (4), vph } \\ & \mathrm{S}(5), \mathrm{vph} \\ & \mathrm{SW}(6), \mathrm{vph} \\ & \mathrm{W}(7), \mathrm{vph} \\ & \mathrm{NW}(8), \mathrm{vph} \\ & \\ \text { Output } \\ \text { Total Vehicles }\end{array}$ |  |  | 32 |  | 11 |  | 79 |  |
|  |  |  |  |  |  |  |  |  |
|  | 7 |  |  |  | 164 |  | 839 |  |
|  |  |  |  |  |  |  |  |  |
|  | 1 |  | 129 |  |  |  | 12 |  |
|  |  |  |  |  |  |  |  |  |
|  | 20 |  | 848 |  | 12 |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  | 28 | 0 | 1009 | 0 | 187 | 0 | 930 | 0 |
| Volume Characteristics | N | NE | E | SE | S | SW | W | NW |
| \% Cars | 97.0\% | 100.0\% | 94.0\% | 100.0\% | 97.0\% | 100.0\% | 94.0\% | 100.0\% |
| \% Heavy Vehicles | 3.0\% | 0.0\% | 6.0\% | 0.0\% | 3.0\% | 0.0\% | 6.0\% | 0.0\% |
| \% Bicycle | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |
| \# of Pedestrians (ped/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| FhV | 0.971 | 1.000 | 0.943 | 1.000 | 0.971 | 1.000 | 0.943 | 1.000 |
| $\mathrm{F}_{\text {ped }}$ | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
|  |  |  |  |  |  |  |  |  |
| Entry/Conflicting Flows | N | NE | E | SE | S | SW | W | NW |
| Flow to Leg \# N (1), pcu/h <br> NE (2), pcu/h <br> E (3), pcu/h <br> SE (4), pcu/h <br> S (5), pcu/h <br> SW (6), pcu/h <br> W (7), pcu/h <br> NW (8), pcu/h <br> Entry flow, pcu/h <br> Conflicting flow, pcu/h | 0 | 0 | 37 | 0 | 12 | 0 | 91 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 8 | 0 | 0 | 0 | 184 | 0 | 967 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 1 | 0 | 149 | 0 | 0 | 0 | 14 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 22 | 0 | 977 | 0 | 13 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 31 | 0 | 1163 | 0 | 209 | 0 | 1072 | 0 |
|  | 1139 | 0 | 117 | 0 | 1066 | 0 | 158 | 0 |

Results: Approach Measures of Effectiveness

Roundabout Analysis Tool
4/21/2020
Single Lane
Version 4.1



局

| Flow to $\mathrm{N}(1), \mathrm{pcu} / \mathrm{h}$ | 0 | 0 | 37 | 0 | 12 | 0 | 91 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Leg \# NE (2), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\mathrm{E}(3), \mathrm{pcu} / \mathrm{h}$ | 8 | 0 | 0 | 0 | 184 | 0 | 967 | 0 |
| SE (4), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\mathrm{S}(5), \mathrm{pcu} / \mathrm{h}$ | 1 | 0 | 149 | 0 | 0 | 0 | 14 | 0 |
| SW (6), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| W (7), pcu/h | 22 | 0 | 977 | 0 | 13 | 0 | 0 | 0 |
| NW (8), pcu/h | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry flow, pcu/h | 31 | 0 | 1163 | 0 | 209 | 0 | 1072 | 0 |
| Entry flow Lane 1, pcu/h | 31 | 0 | 583 | 0 | 26 | 0 | 517 | 0 |
| Entry flow Lane 2, pcu/h | 0 | 0 | 580 | 0 | 184 | 0 | 554 | 0 |
| Conflicting flow, pcu/h | 1139 | 0 | 117 | 0 | 1066 | 0 | 158 | 0 |

Results: Approach Measures of Effectiveness

| HCM 6th Edition | N |  | E |  | S |  | W |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Designations | Lane 1 | Lane 2 | Lane 1 | Lane 2 | Lane 1 | Lane 2 | Lane 1 | Lane 2 |
| Entry Capacity, veh/h | 524 | NA | 1144 | 1213 | 492 | 557 | 1102 | 1172 |
| Entry Flow Rates, veh/h | 30 | NA | 550 | 547 | 25 | 178 | 488 | 523 |
|  | 0.06 | ALC | 0.48 | 0.45 | 0.05 | 0.32 | 0.44 | 0.45 |
| Control Delay, s/veh LOS <br> 95th \% Queue (ft) <br> Approach Delay, LOS | 7.6 |  | 8.4 | 7.6 | 8.0 | 11.1 | 8.1 | 7.8 |
|  | A |  | A | A | A | B | A | A |
|  | 5 |  | 71 | 63 | 4 | 35 | 61 | 62 |
|  | 7.6 sec , LOS A |  | $8 \mathrm{sec}, \mathrm{LOS}$ A |  | 10.7 sec, LOS B |  | 7.9 sec, LOS A |  |
|  | NE |  | SE |  | SW |  | NW |  |
| Lane Designations <br> Entry Capacity, veh/h <br> Entry Flow Rates, veh/h <br> V/C ratio <br> Control Delay, sec/pcu LOS <br> 95th \% Queue (ft) <br> Approach Delay, LOS | Lane 1 | Lane 2 | Lane 1 | Lane 2 | Lane 1 | Lane 2 | Lane 1 | Lane 2 |
|  | NA | NA | NA | NA | NA | NA | NA | NA |
|  | NA | NA | NA | NA | NA | NA | NA | NA |
|  |  |  | A | A |  |  | A1. | A |
|  |  |  | MALU | , ARU |  |  | A | VAE |
|  |  |  |  | A |  |  |  |  |
|  |  |  | A | tat |  |  | Atula | A |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | v 4.0 |
| Bypass Lane Merge Point Analysis (if applicable) |  |  |  |  |  |  |  |  |
| Bypass Characteristics |  |  | Bypass \#1 | $\begin{gathered} \text { Bypass } \\ \# 2 \end{gathered}$ | $\begin{gathered} \text { Bypass } \\ \text { \#3 } \end{gathered}$ | Bypass \#4 | $\begin{gathered} \text { Bypass } \\ \text { \#5 } \end{gathered}$ | $\begin{gathered} \text { Bypass } \\ \# 6 \end{gathered}$ |
| Select Entry Leg from Bypass (FROM) <br> Select Exit Leg for Bypass (TO) <br> Does the bypass have a dedicated receiving lane? \# of Conflicting Exit Flow Lanes |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  | 2 | 2 | 2 | 2 | 2 | 2 |
| Volumes |  |  |  |  |  |  |  |  |
| Entry Leg: Insert Right Turn Volume Exit Leg: (Select Input Method) Lane Flow in Exit Leg*** |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| Sum of inner circulatory flow lane to exit leg (leg bypass merges into) |  |  | N/A | N/A | N/A | N/A | N/A | N/A |
| Sum of outer circulatory flow lane to exit leg (leg bypass merges into) |  |  | N/A | N/A | N/A | N/A | N/A | N/A |
| Critical Lane Flow (Manual) in Exit Leg*** |  |  |  |  |  |  |  |  |
| Volume Characteristics |  |  |  |  |  |  |  |  |
| PHF (Entry Leg) |  |  |  |  |  |  |  |  |

Denorgia Ioppartinemt of Transpoctation
Roundabout Analysis Tool
Multi-Lane

Fhv (Entry Leg)
$F_{\text {ped }}$
PHF (Exit Leg)***
Fhv (Exit Leg)***

|  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |
| N/A | N/A | N/A | N/A | N/A | N/A |
| N/A | N/A | N/A | N/A | N/A | N/A |

***Volume Characteristics are already taken into account for Default method ONLY. Insert Values above if Manual method. Entry/Conflicting Flows Entry Flow
Conflicting Critical Flow

|  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |

## Bypass Lane Results

Entry Capacity of Bypass, veh/h
Flow Rates of Exiting Traffic, veh/h
V/C ratio
Control Delay, sec/pcu
LOS
95th \% Queue (ft)

|  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## Geogia Department of Transportation

SR 3 @ Old Dixie HWY/ Five Springs Rd with Right Turn Reduction
Signal Warrants - Summary

## Major Street Approaches

Eastbound: SR 3
Number of Lanes: 2
Approach Speed: 55
Total Approach Volume: 6,594
Westbound: SR 3
Number of Lanes: 2
Approach Speed: 55
Total Approach Volume: 7,676

## Minor Street Approaches

Northbound: Old Dixie HWY
Number of Lanes: 1
Total Approach Volume: 233
Southbound: 5 Springs Rd
Number of Lanes: 1
Total Approach Volume: 175

## Warrant Summary (Urban values apply.)

Warrant 1 - Eight Hour Vehicular Volumes Not Satisfied
Warrant 1A - Minimum Vehicular Volume Not Satisfied
Required volumes reached for 0 hours, 8 are needed
Warrant 1B - Interruption of Continuous Traffic .Not Satisfied
Required volumes reached for 0 hours, 8 are needed
Warrant 1 A\&B - Combination of Warrants Not Satisfied
Required volumes reached for 0 hours, 8 are needed
Warrant 2 - Four Hour Volumes Not Satisfied
Number of hours (0) volumes exceed minimum < minimum required (4).
Warrant 3 - Peak Hour ..... Not Satisfied
Warrant 3A - Peak Hour Delay Not Satisfied
Total approach volumes and delays on minor street do not exceed minimums for any hour.
Warrant 3B - Peak Hour Volumes Not Satisfied
Volumes do not exceed minimums for any hour.
Warrant 4 - Pedestrian Volumes ..... Not SatisfiedRequired 4 Hr pedestrian volume reached for 0 hour(s) and the single hour volume for 0 hour(s)
Warrant 5 - School Crossing Not Satisfied
Number of gaps $>.0$ seconds ( 0 ) exceeds the number of minutes in the crossing period ( 0 ).
Warrant 6 - Coordinated Signal System ..... Not Satisfied
No adjacent coordinated signals are present
Warrant 7 - Crash Experience ..... Not Satisfied
Number of accidents ( -1 ) is less than minimum (5). Volume minimums are not met.
Warrant 8 - Roadway Network ..... Not Satisfied
Major Route conditions not met. One or more volume requirement met.

## SR 3 @ Old Dixie HWY/ Five Springs Rd

 with Right Turn Reduction
## Signal Warrants - Summary



Analysis of 8-Hour Volume Warrants:

| Hour <br> Begin | Major <br> Total | Higher Minor |  | War-1A |  |  | War-1B |  |  | War-1A\&B |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Vol | Dir | Major Crit | Minor Crit | Meets? | Major Crit | Minor Crit | Meets? | Major Crit | Minor Crit | Meets? |
| 00:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 01:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 02:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 03:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 04:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 05:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 06:00 | 1,413 | 17 | SB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 07:00 | 1,939 | 23 | NB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 08:00 | 1,244 | 16 | NB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 09:00 | 766 | 19 | NB | 600-Yes | 150-No | Major | 900-No | 75-No | --- | 720-Yes | 120-No | Major |
| 10:00 | 731 | 17 | NB | 600-Yes | 150-No | Major | 900-No | 75-No | --- | 720-Yes | 120-No | Major |
| 11:00 | 877 | 18 | NB | 600-Yes | 150-No | Major | 900-No | 75-No | --- | 720-Yes | 120-No | Major |
| 12:00 | 957 | 26 | NB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 13:00 | 988 | 23 | SB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 14:00 | 1,103 | 23 | NB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 15:00 | 1,364 | 27 | NB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 16:00 | 1,322 | 17 | NB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 17:00 | 1,566 | 23 | SB | 600-Yes | 150-No | Major | 900-Yes | 75-No | Major | 720-Yes | 120-No | Major |
| 18:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 19:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 20:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 21:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 22:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |
| 23:00 | 0 | 0 | NB | 600-No | 150-No | --- | 900-No | 75-No | --- | 720-No | 120-No | --- |



## HCS7 All-Way Stop Control Report

General Information

| Analyst | Manara Ali |
| :--- | :--- |
| Agency/Co. | GDOT |
| Date Performed | $11 / 26 / 2019$ |
| Analysis Year | 2019 |
| Analysis Time Period (hrs) | 0.25 |
| Time Analyzed | Peak Hour |
| Project Description | AWSC |

Site Information

| Intersection | SR 3 @ Old Dixie HWY |
| :--- | :--- |
| Jurisdiction | D6- Traffi Operations |
| East/West Street | SR 3 |
| North/South Street | Oldi Dixie HWY |
| Peak Hour Factor | 0.92 |
|  |  |

Lanes


Vehicle Volume and Adjustments

| Approach | Eastbound |  |  | Westbound |  |  | Northbound |  |  | Southbound |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | L | T | R | L | T | R | L | T | R | L | T | R |
| Volume | 79 | 839 |  | 129 | 848 |  | 12 | 11 | 164 | 7 | 0 | 20 |
| \% Thrus in Shared Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane | L1 | L2 | L3 | L1 | L2 | L3 | L1 | L2 | L3 | L1 | L2 | L3 |
| Configuration | L | T | T | L | T | T | LT | R |  | LT | R |  |
| Flow Rate, v (veh/h) | 86 | 456 | 456 | 140 | 461 | 461 | 25 | 178 |  | 8 | 22 |  |
| Percent Heavy Vehicles | 6 | 0 | 0 | 6 | 0 | 0 | 3 | 3 |  | 3 | 3 |  |

## Departure Headway and Service Time

| Initial Departure Headway, hd (s) | 3.20 | 3.20 | 3.20 | 3.20 | 3.20 | 3.20 | 3.20 | 3.20 | 3.20 | 3.20 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Initial Degree of Utilization, x | 0.076 | 0.405 | 0.405 | 0.125 | 0.410 | 0.410 | 0.022 | 0.158 | 0.007 | 0.019 |  |
| Final Departure Headway, hd (s) | 8.95 | 8.35 | 8.35 | 8.84 | 8.24 | 8.24 | 11.32 | 10.36 | 12.24 | 11.04 |  |
| Final Degree of Utilization, $x$ | 0.213 | 1.057 | 1.057 | 0.344 | 1.055 | 1.055 | 0.079 | 0.513 | 0.026 | 0.067 |  |
| Move-Up Time, m (s) | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 |  |
| Service Time, ts (s) | 6.65 | 6.05 | 6.05 | 6.54 | 5.94 | 5.94 | 9.02 | 8.06 | 9.94 | 8.74 |  |

Capacity, Delay and Level of Service

| Flow Rate, v (veh/h) | 86 | 456 | 456 | 140 | 461 | 461 | 25 | 178 | 8 | 22 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity | 402 | 431 | 431 | 407 | 437 | 437 | 318 | 347 | 294 | 326 |  |
| 95\% Queue Length, Q ${ }_{95}$ (veh) | 0.8 | 14.7 | 14.7 | 1.5 | 14.7 | 14.7 | 0.3 | 2.8 | 0.1 | 0.2 |  |
| Control Delay (s/veh) | 14.1 | 88.2 | 88.2 | 16.1 | 87.0 | 87.0 | 15.0 | 23.5 | 15.3 | 14.5 |  |
| Level of Service, LOS | B | F | F | C | F | F | B | C | C | B |  |
| Approach Delay (s/veh) |  | 81.8 |  |  | 77.7 |  |  | 22.4 |  | 14.7 |  |
| Approach LOS |  | F |  |  | F |  |  | C |  | B |  |
| Intersection Delay, s/veh \| LOS | 73.8 |  |  |  |  |  | F |  |  |  |  |

HCS7 Alternative Intersections Results Summary

## General Information

| Agency | GD |
| :--- | :--- |
| Analyst | M |
| Jurisdiction | D |
| Intersection | SR |
| Main Intersection File | RC |
| West Crossover File | R |
| East Crossover File | RC |
| Project Description | R- |

Alternative Intersection Information

| GDOT | Analysis Date | $12 / 23 / 2019$ |
| :--- | :--- | :--- |
| Manara Ali | Duration, h | 0.25 |
| D6- Traffic Operations | PHF | 0.92 |
| SR 3 @ Old Dixie Hwy |  |  |
| RCUT ASIS.xtw |  |  |
| RCUT WB Crossover.xtw |  |  |
| RCUT EB Crossover.xtw |  |  |
| R-CUT |  |  |

Intersection Type

| EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 930 |  | 8 |  | 880 |  |  |  |  |  |  |  |  |  |
| 0 | 79 | 846 | 13 | 0 | 129 | 860 | 43 |  |  |  | 187 |  |  |  | 28 |
| 23 |  | 1010 |  |  |  | 1009 |  |  |  |  |  |  |  |  |  |

(1) West Crossover

(2) Main Intersection

(3) East Crossover


| Queue-to-Storage Ratio | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection One (RQ) |  |  |  |  | 0.01 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Two (Ra) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Three (RQ) | 0.02 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Alternative Intesection Results

| O-D | O-D Movements | Flow Rate (veh/h) | Control Delay (s/veh) | EDTT (s/veh) | ETT (s/veh) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EBL | EBL(2) | 86 | 10.8 | -- | 10.8 | B |
| EBT | -- | 912 | 0.0 | -- | 0.0 | A |
| EBR | -- | 13 | 0.0 | -- | 0.0 | A |
| WBL | WBL(2) | 140 | 11.3 | -- | 11.3 | B |
| WBT | -- | 922 | 0.0 | -- | 0.0 | A |
| WBR | -- | 35 | 0.0 | -- | 0.0 | A |
| NBL | NBR(2) + EBU(3) | 13 | 15.5 | 17.3 | 32.8 | C |
| NBT | NBR(2) + EBU(3) | 12 | 15.5 | 17.3 | 32.8 | C |
| NBR | NBR(2) | 178 | 15.5 | -- | 15.5 | B |
| SBL | SBR(2) + WBU(1) | 8 | 12.1 | 17.3 | 29.4 | C |
| SBT | SBR(2) + WBU(1) | 1 | 12.1 | 17.3 | 29.4 | C |
| SBR | SBR(2) | 22 | 12.1 | -- | 12.1 | B |


| Overall Results | EB |  | WB |  | NB |  | SB |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach ETT, s/veh \| LOS | 0.9 | A | 1.4 | A | 17.6 | B | 17.1 | B |
| Intersection ETT, s/veh \| LOS | 2.8 |  |  |  | A |  |  |  |

All Traffic Data
ㄱ - - =-nexiolo11
(303) 216-2439
www.alltrafficdata.net

Location: \#4 Old Dixie Hwy \& SR 3 AM
Date and Start Time: Wednesday, October 9, 2019
Peak Hour: 07:00 AM - 08:00 AM
Peak 15-Minutes: 07:45 AM - 08:00 AM


Note: Total study counts contained in parentheses.
Traffic Counts

| Interval | SR 3 <br> Eastbound |  |  |  | SR 3 <br> Westbound |  |  |  | Old Dixie Hwy Northbound |  |  |  | 5 Springs Rd Southbound |  |  |  | Total | Rolling Hour | Pedestrain Crossings |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  | West | East | South | North |
| 6:00 AM | 0 | 7 | 59 | 1 | 0 | 14 | 91 | 2 | 0 | 3 | 6 | 35 | 0 | 1 | 4 | 2 | 225 | 1,601 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 20 | 110 | 6 | 0 | 28 | 139 | 3 | 0 | 1 | 0 | 29 | 0 | 2 | 2 | 1 | 341 | 1,874 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 20 | 164 | 11 | 0 | 47 | 209 | 7 | 0 | 1 | 1 | 38 | 0 | 1 | 0 | 6 | 505 | 1,981 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 30 | 170 | 8 | 0 | 64 | 196 | 7 | 0 | 1 | 2 | 41 | 0 | 1 | 6 | 4 | 530 | 2,065 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 10 | 208 | 3 | 0 | 37 | 163 | 8 | 0 | 5 | 6 | 49 | 0 | 2 | 0 | 7 | 498 | 2,155 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 9 | 171 | 5 | 0 | 31 | 187 | 5 | 0 | 3 | 0 | 29 | 0 | 2 | 1 | 5 | 448 | 2,130 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 26 | 223 | 3 | 0 | 29 | 247 | 7 | 0 | 3 | 2 | 43 | 0 | 1 | 0 | 5 | 589 | 2,070 | 0 | 0 | 0 | 2 |
| 7:45 AM | 0 | 34 | 237 | 1 | 0 | 32 | 251 | 12 | 0 | 1 | 3 | 43 | 1 | 2 | 0 | 3 | 620 | 1,749 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 25 | 227 | 2 | 0 | 27 | 149 | 9 | 0 | 1 | 0 | 26 | 0 | 4 | 0 | 3 | 473 | 1,376 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 11 | 177 | 2 | 0 | 15 | 142 | 4 | 0 | 1 | 3 | 23 | 0 | 2 | 0 | 8 | 388 | 1,127 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 12 | 105 | 1 | 0 | 17 | 94 | 1 | 0 | 4 | 4 | 20 | 0 | 4 | 0 | 6 | 268 | 985 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 11 | 117 | 1 | 0 | 20 | 74 | 1 | 0 | 2 | 1 | 16 | 0 | 2 | 0 | 2 | 247 | 917 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 9 | 83 | 4 | 0 | 16 | 83 | 0 | 0 | 1 | 3 | 16 | 0 | 1 | 3 | 5 | 224 | 889 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 6 | 95 | 1 | 0 | 15 | 97 | 3 | 0 | 3 | 2 | 17 | 0 | 1 | 1 | 5 | 246 | 849 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 4 | 71 | 3 | 0 | 12 | 77 | 2 | 0 | 3 | 1 | 21 | 0 | 1 | 1 | 4 | 200 | 814 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 5 | 76 | 4 | 0 | 11 | 84 | 5 | 0 | 3 | 3 | 19 | 2 | 1 | 2 | 4 | 219 | 861 | 0 | 0 | 0 | 0 |
| 10:00 AM | 0 | 4 | 71 | 5 | 0 | 12 | 60 | 2 | 0 | 0 | 1 | 17 | 0 | 7 | 0 | 5 | 184 | 851 | 0 | 0 | 0 | 0 |
| 10:15 AM | 0 | 4 | 69 | 4 | 0 | 18 | 87 | 4 | 0 | 2 | 4 | 15 | 0 | 1 | 1 | 2 | 211 | 895 | 0 | 0 | 0 | 0 |
| 10:30 AM | 0 | 7 | 93 | 1 | 0 | 8 | 96 | 2 | 0 | 4 | 4 | 22 | 0 | 1 | 3 | 6 | 247 | 934 | 0 | 0 | 0 | 0 |
| 10:45 AM | 0 | 5 | 82 | 2 | 0 | 15 | 79 | 1 | 0 | 1 | 1 | 13 | 0 | 1 | 2 | 7 | 209 | 953 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 6 | 77 | 6 | 0 | 16 | 91 | 2 | 0 | 1 | 1 | 21 | 0 | 1 | 0 | 6 | 228 | 1,005 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 4 | 96 | 5 | 0 | 14 | 87 | 4 | 0 | 6 | 1 | 18 | 0 | 3 | 3 | 9 | 250 | 1,069 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 5 | 97 | 4 | 0 | 12 | 112 | 1 | 0 | 4 | 3 | 15 | 0 | 4 | 1 | 8 | 266 | 1,065 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 6 | 104 | 2 | 0 | 26 | 99 | 1 | 0 | 2 | 0 | 15 | 0 | 1 | 0 | 5 | 261 | 1,068 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 4 | 122 | 6 | 0 | 13 | 111 | 5 | 0 | 5 | 2 | 17 | 0 | 0 | 2 | 5 | 292 | 1,071 | 0 | 0 | 0 | 0 |
| 12:15 PM | 0 | 5 | 104 | 7 | 0 | 15 | 90 | 4 | 0 | 4 | 0 | 9 | 0 | 3 | 1 | 4 | 246 | 1,070 | 0 | 0 | 0 | 0 |
| 12:30 PM | 0 | 3 | 109 | 5 | 0 | 22 | 94 | 2 | 0 | 7 | 3 | 11 | 0 | 2 | 2 | 9 | 269 | 1,083 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 4 | 98 | 2 | 0 | 19 | 110 | 3 | 0 | 2 | 3 | 21 | 0 | 0 | 0 | 2 | 264 | 1,107 | 0 | 0 | 0 | 0 |
| 1:00 PM | 0 | 2 | 113 | 5 | 0 | 31 | 99 | 4 | 0 | 2 | 2 | 27 | 0 | 1 | 0 | 5 | 291 | 1,136 | 0 | 0 | 0 | 0 |
| 1:15 PM | 0 | 3 | 99 | 2 | 0 | 24 | 95 | 3 | 0 | 1 | 1 | 23 | 0 | 2 | 1 | 5 | 259 | 1,146 | 0 | 0 | 0 | 0 |
| 1:30 PM | 0 | 7 | 96 | 6 | 0 | 30 | 113 | 2 | 0 | 5 | 2 | 22 | 0 | 2 | 7 | 1 | 293 | 1,207 | 0 | 0 | 0 | 0 |
| 1:45 PM | 0 | 7 | 102 | 3 | 0 | 37 | 102 | 3 | 0 | 2 | 4 | 16 | 0 | 2 | 8 | 7 | 293 | 1,251 | 0 | 0 | 0 | 0 |
| 2:00 PM | 0 | 5 | 92 | 2 | 0 | 19 | 114 | 1 | 0 | 1 | 9 | 47 | 0 | 2 | 3 | 6 | 301 | 1,284 | 0 | 0 | 0 | 0 |
| 2:15 PM | 0 | 7 | 120 | 5 | 0 | 30 | 117 | 3 | 0 | 2 | 5 | 25 | 0 | 1 | 0 | 5 | 320 | 1,480 | 0 | 0 | 0 | 0 |
| 2:30 PM | 0 | 9 | 125 | 5 | 0 | 22 | 136 | 7 | 0 | 0 | 2 | 20 | 0 | 3 | 3 | 5 | 337 | 1,520 | 0 | 0 | 0 | 0 |


| 2:45 PM | 0 | 9 | 94 | 5 | 0 | 35 | 138 | 3 | 0 | 3 | 1 | 22 | 0 | 2 | 7 | 7 | 326 | 1,605 | 0 | 0 | 0 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3:00 PM | 0 | 5 | 195 | 3 | 0 | 28 | 142 | 4 | 0 | 9 | 3 | 84 | 0 | 1 | 0 | 23 | 497 | 1,641 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 5 | 148 | 2 | 0 | 34 | 120 | 5 | 0 | 0 | 4 | 30 | 0 | 1 | 4 | 7 | 360 | 1,575 | 0 | 0 | 0 | 0 |
| 3:30 PM | 0 | 4 | 160 | 5 | 0 | 41 | 148 | 6 | 0 | 1 | 6 | 38 | 0 | 1 | 1 | 11 | 422 | 1,529 | 0 | 0 | 0 | 0 |
| 3:45 PM | 0 | 1 | 114 | 1 | 0 | 33 | 155 | 5 | 0 | 1 | 3 | 28 | 0 | 5 | 1 | 15 | 362 | 1,508 | 0 | 0 | 0 | 0 |
| 4:00 PM | 0 | 1 | 141 | 6 | 0 | 44 | 185 | 6 | 0 | 1 | 5 | 23 | 0 | 1 | 0 | 18 | 431 | 1,502 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 1 | 92 | 3 | 0 | 29 | 154 | 3 | 0 | 1 | 2 | 22 | 0 | 1 | 0 | 6 | 314 | 1,713 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 6 | 169 | 2 | 0 | 43 | 124 | 2 | 0 | 1 | 4 | 35 | 0 | 2 | 3 | 10 | 401 | 1,808 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 2 | 130 | 2 | 0 | 22 | 154 | 1 | 0 | 2 | 1 | 28 | 0 | 0 | 0 | 14 | 356 | 1,837 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 4 | 236 | 7 | 0 | 49 | 262 | 8 | 0 | 1 | 1 | 32 | 0 | 3 | 0 | 39 | 642 | 1,804 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 4 | 124 | 4 | 0 | 39 | 177 | 1 | 0 | 3 | 1 | 32 | 0 | 1 | 7 | 16 | 409 |  | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 2 | 152 | 2 | 0 | 34 | 170 | 3 | 0 | 2 | 3 | 46 | 0 | 3 | 4 | 9 | 430 |  | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 119 | 3 | 0 | 23 | 139 | 4 | 0 | 2 | 0 | 24 | 0 | 3 | 2 | 4 | 323 |  | 0 | 0 | 0 | 0 |

## Peak Rolling Hour Flow Rates

| Vehicle Type | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |
| Articulated Trucks | 0 | 4 | 50 | 0 | 0 | 0 | 52 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 | 111 |
| Lights | 0 | 75 | 757 | 12 | 0 | 122 | 770 | 31 | 0 | 10 | 11 | 153 | 1 | 7 | 1 | 16 | 1,966 |
| Mediums | 0 | 0 | 32 | 0 | 0 | 7 | 26 | 1 | 0 | 1 | 0 | 11 | 0 | 0 | 0 | 0 | 78 |
| Total | 0 | 79 | 839 | 12 | 0 | 129 | 848 | 32 | 0 | 12 | 11 | 164 | 1 | 7 | 1 | 20 | 2,155 |



| $\begin{gathered} \text { Accident } \\ \text { No } \end{gathered}$ | Date | Time | Injuries | Fatalities | Manner of Collision | Light | Surface | LatDec | LongDec |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5151884 | 1/29/2015 | 7:50:00 | 0 | 0 | Rear End | Daylight | Dry | 34.70 | -84.97 |
| 5245257 | 4/5/2015 | 20:59:00 | 3 | 0 | Angle | DarkNot Lighted | Dry | 34.70 | -84.97 |
| 5368438 | 7/21/2015 | 6:33:00 | 1 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 5400361 | 8/22/2015 | 13:44:00 | 1 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 5497568 | 11/4/2015 | 12:28:00 | 0 | 0 | Rear End | Daylight | Dry | 34.70 | -84.97 |
| 5531848 | 10/16/2015 | 11:01:00 | 0 | 0 | Side-Swipe | Daylight | Dry | 34.70 | -84.97 |
| 5917302 | 9/13/2016 | 6:40:00 | 0 | 0 | Angle | DarkNot Lighted | Dry | 34.70 | -84.97 |
| 6149505 | 3/13/2017 | 6:10:00 | 0 | 0 | Rear End | DarkNot Lighted | Dry | 34.70 | -84.97 |
| 6342159 | 8/5/2017 | 10:54:00 | 0 | 0 | Rear End | Daylight | Dry | 34.70 | -84.97 |
| 6432561 | 10/17/2017 | 16:11:00 | 0 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 6567813 | 1/25/2018 | 5:52:00 | 2 | 0 | Angle | DarkNot Lighted | Dry | 34.70 | -84.97 |
| 6644288 | 3/21/2018 | 6:52:00 | 3 | 0 | Angle | DarkNot Lighted | Dry | 34.70 | -84.97 |
| 6714617 | 5/15/2018 | 7:52:00 | 0 | 0 | Rear End | Daylight | Dry | 34.70 | -84.97 |
| 6724009 | 5/24/2018 | 17:19:00 | 1 | 0 | Rear End | Daylight | Dry | 34.70 | -84.97 |
| 6749549 | 6/13/2018 | 7:05:00 | 1 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 6770840 | 6/26/2018 | 17:17:00 | 1 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 7073523 | 2/1/2019 | 6:52:00 | 0 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 7126771 | 3/15/2019 | 8:06:00 | 0 | 0 | Angle | Daylight | Wet | 34.70 | -84.97 |
| 7139586 | 3/25/2019 | 17:11:00 | 0 | 0 | Rear End | Daylight | Wet | 34.70 | -84.97 |
| 7189618 | 4/24/2019 | 15:10:00 | 1 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 7213258 | 5/18/2019 | 11:10:00 | 3 | 0 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 7238760 | 6/6/2019 | 6:35:00 | 0 | 0 | Rear End | Dawn | Dry | 34.70 | -84.97 |
| 7253929 | 6/13/2019 | 17:30:00 | 1 | 1 | Angle | Daylight | Dry | 34.70 | -84.97 |
| 7295765 | 7/23/2019 | 17:09:00 | 0 | 0 | Rear End | Daylight | Dry | 34.70 | -84.97 |
| 7467020 | 12/5/2019 | 22:12:00 | 0 | 0 | Angle | DarkNot Lighted | Dry | 34.70 | -84.97 |
| 7480817 | 12/11/2019 | 17:08:00 | 1 | 0 | Rear End | Daylight | Dry | 34.70 | -84.97 |
| 7481779 | 12/15/2019 | 6:45:00 | 1 | 0 | Angle | DarkNot Lighted | Dry | 34.70 | -84.97 |
| 7585029 | 1/13/2020 | 23:07:00 | 0 | 0 | Rear End | DarkNot Lighted | Wet | 34.70 | -84.97 |


[^0]:    Conclusions/Comments:

[^1]:    Note: Stage 2 score is not given (shown as "-") if signal or AWS is selected as control type but respective warrants are not met

